

التيار المستمر

2.1 Uncontrolled Single phase half wave rectifier
 2.1.1 Resistive load

neglecting voltage drop across diode

$$V_o = \frac{1}{2\pi} \int_0^{\pi} V_m \sin \omega t \, d\omega t$$

$$= \frac{V_m}{2\pi} (-\cos \omega t)_0^{\pi}$$

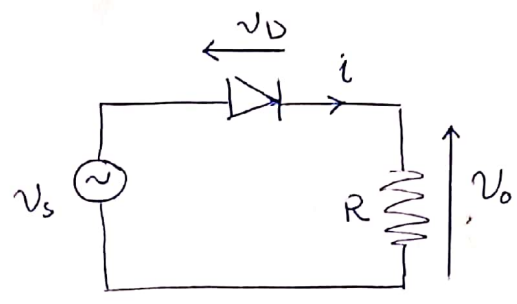
$$= \frac{V_m}{\pi}$$

$$i = v_o / R$$

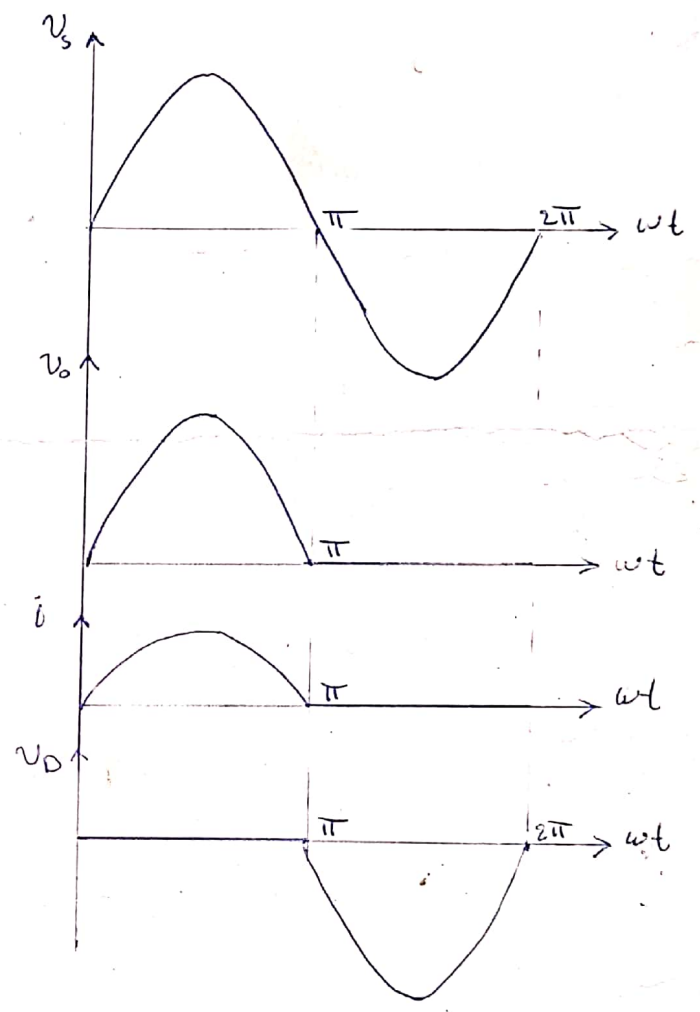
$$I = V_o / R$$

if voltage drop is not neglected then

$$V_o = \frac{V_m}{\pi} - V_D \quad (2.1)$$



(a)



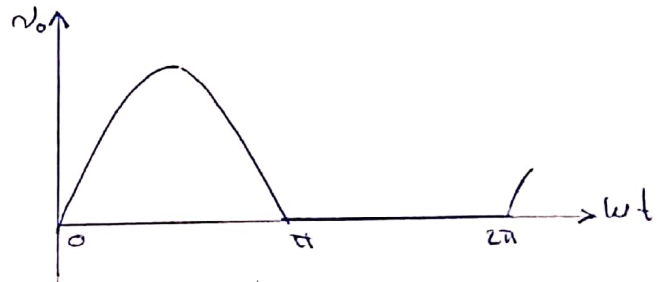
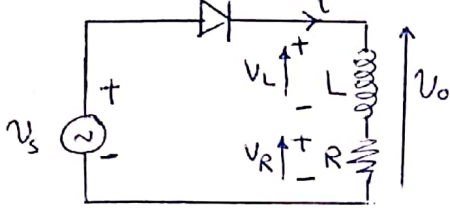
(b)

Fig.(2.1)

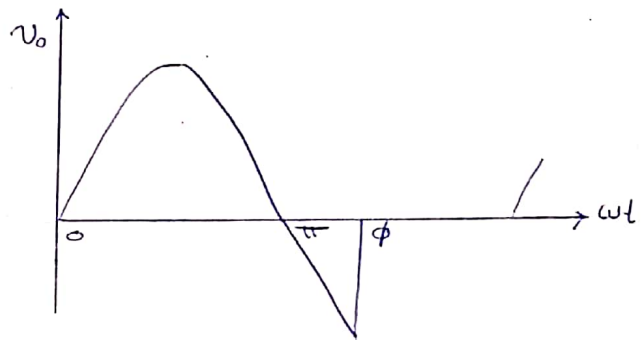
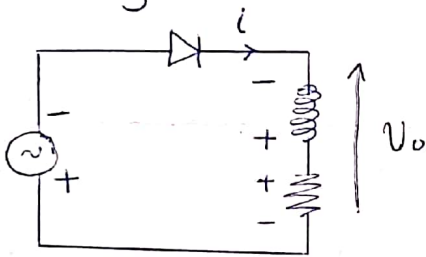
2.1.2 Inductive load

إن الحمل المحثاد هو حمل عثي Inductive load يتكون من (pure inductance + pure resistance) إن د (pure inductance) لا تستهلك الطاقة فثي الكثر الموجب من فولتية المصدر المتناوبه تفترنا الطاقة وفي كثر السالب ترفع هذه الطاقة المخزونه إلى المصدر وكالتالي:

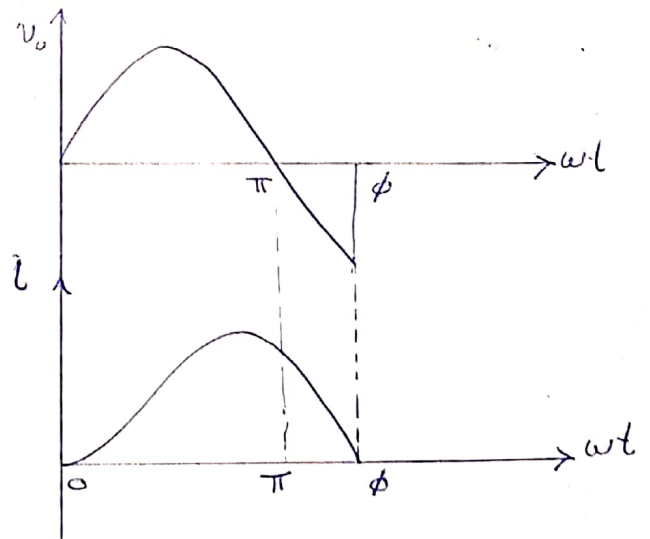
1) During +ve half cycle



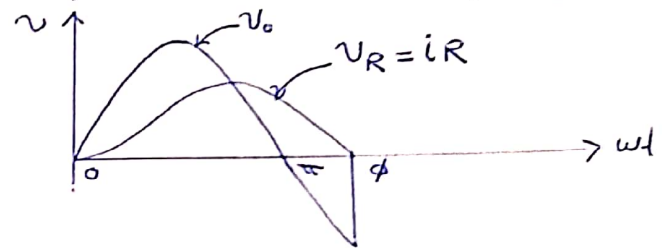
2) During -ve half cycle



ايه ان المحاثه سوف ترفع الطاقة إلى المصدر ولقربنا ارجاع هذه الطاقة فإن المحاثه سوف تحكس قطبيتها وتسر التيار بنفس اتجاه التيار في الكثر الموجب إلى ان تستهلك الطاقة المخزونه في المحاثه عند الزاويه ϕ اذن فإن التيار يمر خلال القتره $[\phi]$ وكالتالي:



ان الفولتية غير المتقاومة R ستكون بنفس الطور مع التيار، وبالتالي

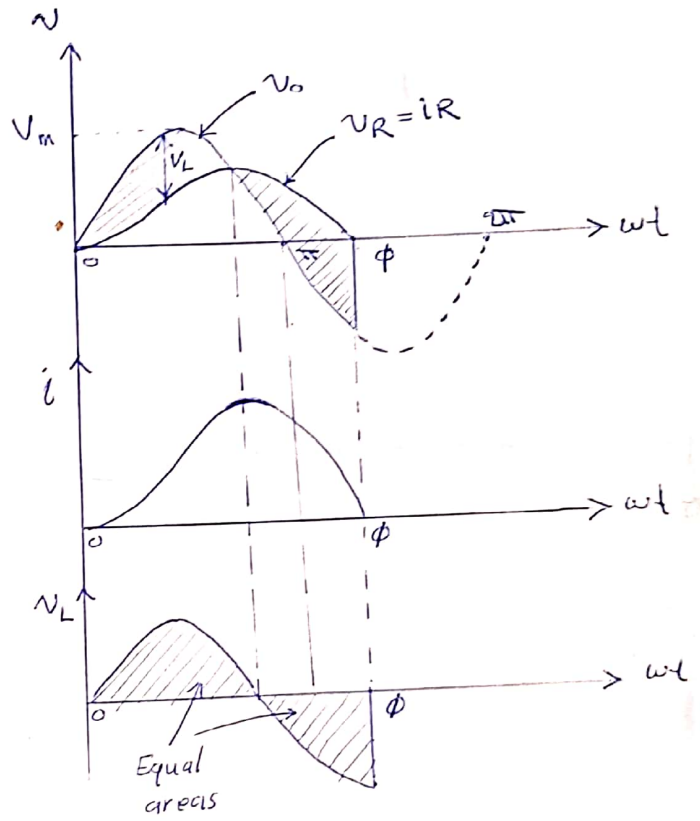


وان الفرت بينه v_o و v_R هو v_L وذلك لأن $v_o = v_R + v_L$. الآن نستطيع جمع هذه الاشكال في شكل واحد (Fig. (2.2))

$$v_o = \frac{1}{2\pi} \int_0^\phi V_m \sin \omega t \, d\omega t$$

$$= \frac{V_m}{2\pi} (-\cos \omega t)^\phi$$

$$= \frac{V_m}{2\pi} (1 - \cos \phi) \quad \text{--- (2.2)}$$



ϕ can be calculated from Fig (2.3) below

Where $\theta = \tan^{-1} \frac{\omega L}{R}$

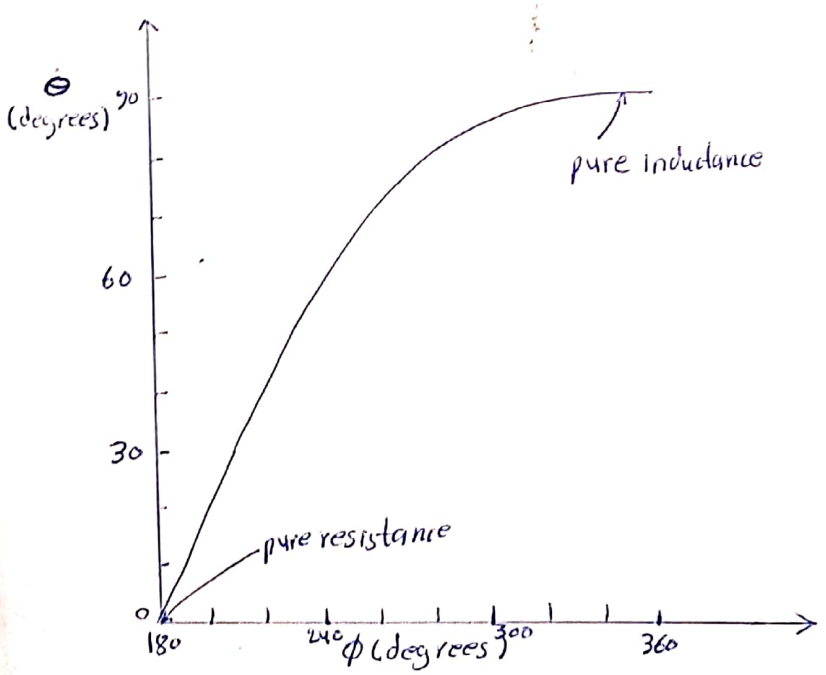


Fig (2.2)

Fig. (2.3)

$$V_m \sin \omega t = Ri + L di/dt$$

$i(t) = i_t + i_{ss}$ where i_t = transient current, i_{ss} = steady state current

$$i_{ss} = \frac{V_m}{\sqrt{R^2 + (\omega L)^2}} \sin(\omega t - \theta)$$

$$= \frac{V_m}{Z} \sin(\omega t - \theta)$$

where $Z = \sqrt{R^2 + (\omega L)^2}$, $\theta = \tan^{-1}(\omega L/R)$

$$i_t = A e^{-\frac{R}{L}t}$$

$$i(0) = 0 = i_t(0) + i_{ss}(0)$$

i.e. at $t=0$ the current i is zero.

$$A e^0 + \frac{V_m}{Z} \sin(0 - \theta) = 0 \Rightarrow A - \frac{V_m}{Z} \sin \theta = 0$$

$$\Rightarrow A = \frac{V_m}{Z} \sin \theta$$

$$i(t) = i_t + i_{ss}$$

$$= \frac{V_m}{Z} \left[\sin(\omega t - \theta) + \sin \theta e^{-\frac{R}{L}t} \right]$$

$$\therefore i(t) = \frac{V_m}{Z} \left[\sin(\omega t - \theta) + \sin \theta e^{-\frac{\omega t}{\tan \theta}} \right] \quad \text{--- (2.3)}$$

2.1.3 Inductive load with freewheeling diode

$$V_o = \frac{1}{2\pi} \int_0^{\pi} V_m \sin \omega t \, d\omega t$$

$$= \frac{V_m}{\pi}$$

$$I_{o2\pi} = \frac{V_m}{Z} \sin \theta \frac{1 + e^{-\frac{\pi}{\tan \theta}}}{e^{-\frac{\pi}{\tan \theta}} - 1} \quad \text{--- (2.4)}$$

$$I_{o1\pi} = I_{o2\pi} e^{-\frac{\pi}{\tan \theta}} \quad \text{--- (2.5)}$$

1- $0 \leq \omega t \leq \pi$

$$i_a = i = \frac{V_m}{Z} \sin(\omega t - \theta) + (I_{o2\pi} + \frac{V_m}{Z} \sin \theta) e^{-\frac{\omega t}{\tan \theta}} \quad \text{--- (2.6)}$$

2- $\pi \leq \omega t \leq 2\pi$

$$i_o = i_{df} = I_{o1\pi} e^{-\frac{(\omega t - \pi)}{\tan \theta}} \quad \text{--- (2.7)}$$

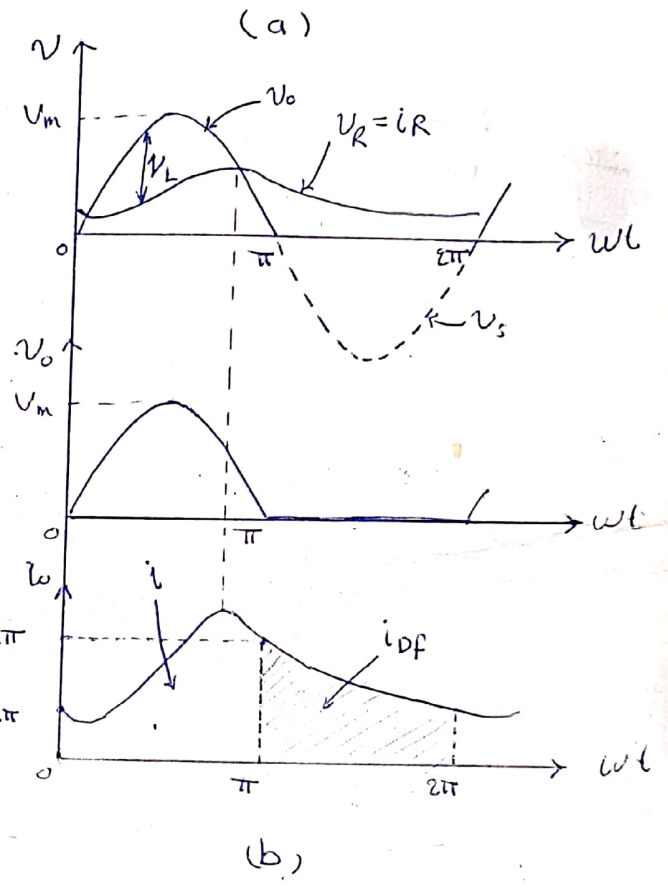
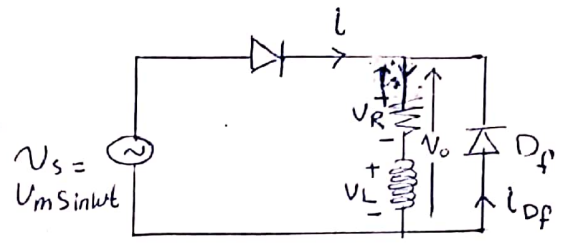


Fig. (2.4)

Example: In the circuit of figure (2.4a) the source voltage is $240\sqrt{2} \sin(2\pi 50t) \text{ V}$, $R = 10 \text{ ohms}$ and $L = 50 \text{ mH}$. Calculate

- the mean value of the load current I_o
- the current boundary conditions $I_{o1\pi}$, $I_{o2\pi}$.
- find $i_a(t)$ at $\omega t = \pi/3$ & $\omega t = 4\pi/3$

Solution

(a)

$$V_o = \frac{V_m}{\pi}$$

$$= \frac{\sqrt{2} \times 240}{\pi}$$

$$= 108 \text{ V}$$

$$I_o = \frac{V_o}{R}$$

$$= \frac{108}{10}$$

$$= 10.8 \text{ A}$$

(b)

$$Z = \sqrt{R^2 + (\omega L)^2}$$

$$= \sqrt{(10)^2 + (2\pi \times 50 \times 50 \times 10^{-3})^2}$$

$$= 18.62 \Omega$$

$$\tan \theta = \frac{X_L}{R} = \frac{2\pi \times 50 \times 50 \times 10^{-3}}{10} = 1.57$$

$$\theta = \tan^{-1}(1.57)$$

$$= 57.5^\circ = \frac{57.5 \pi}{180} \text{ rad} = 0.319\pi$$

$$\sin \theta = 0.844 \quad -\pi/\tan \theta$$

$$I_{o2\pi} = \frac{V_m}{Z} \sin \theta \frac{1 + e^{-\pi/\tan \theta}}{e^{\pi/\tan \theta} - e^{-\pi/\tan \theta}}$$

$$= \frac{240\sqrt{2}}{18.62} \times 0.844 \times \frac{1 + 0.135}{7.389 - 0.135}$$

$$= 2.4 \text{ A}$$

$$I_{o1\pi} = I_{o2\pi} e^{\pi/\tan \theta}$$

$$= 2.4 e^{\pi/1.57}$$

$$= 17.73 \text{ A}$$

(c)

at $\omega t = \pi/3$:

$$i_o(t) = \frac{V_m}{Z} \sin(\omega t - \theta) + (I_{o2\pi} + \frac{V_m}{Z} \sin \theta) e^{-\frac{\omega t}{\tan \theta}}$$

$$\Rightarrow i_o = \frac{240\sqrt{2}}{18.62} \sin(\frac{\pi}{3} - 0.319\pi) + (2.4 + \frac{240\sqrt{2}}{18.62} \sin 0.319\pi) e^{-\frac{\pi/3}{1.57}}$$

$$= 18.23 \sin(0.0143\pi) + (2.4 + 18.23 \sin 0.319\pi) e^{-0.667}$$

$$= 0.8187 + (2.4 + 15.36) \times 0.5132$$

$$= 9.933 \text{ A}$$

at $\omega t = 4\pi/3$:

$$i_o(t) = I_{o1\pi} e^{-\frac{(\omega t - \pi)}{\tan \theta}}$$

$$\Rightarrow i_o = 17.73 e^{-\frac{(4\pi/3 - \pi)}{1.57}}$$

$$= 17.73 e^{-\frac{0.333\pi}{1.57}}$$

$$= 17.73 \times 0.5136$$

$$= 9.1 \text{ A}$$