

# **Plates and Shells**

## **Course Description:**

This course covers the mechanics of plates using classical theory (cylindrical bending, rectangular plates, and circular plates) and plate theory with shear deformation. Includes combined effects of bending and in-plane forces, membrane theory of shells, analysis of thin cylindrical shells of revolution, and general theory of thin elastic shells.

## **Topics Covered:**

1. Introduction

### **THIN ELASTIC PLATES**

2. Governing Equations of Small Deflection Plate Theory

3. Analytical Solutions for Rectangular Plates

4. Analytical Solutions for Circular Plates

5. Large Deflection Theory of Plates

### **THIN ELASTIC SHELLS**

7. Introduction

8. Geometry of the middle surface

9. General Theory of Shells

10. Membrane theory of shells

11. Bending Theory of Shells

## References

- Theory of Plates and Shells, S.P. Timoshenko and S. Woinowsky-Krieger, McGraw-Hill Book Company, NY. 2<sup>nd</sup> edition 1959, reissued 1987 (QA931 .T56 1959)
- Stresses in Shells. W. Flügge, Springer-Verlag, Berlin, 2nd Edition, 1960, 2nd printing, 1990 (TA660.S5 F58 1973).
- Beams, Plates and Shells, L.H. Donnell, McGraw-Hill Book Company, NY., 1976 (TA660.B4 D66)
- Shell Theory, F. I. Niordson, North-Holland, Amsterdam, 1985 (TA660.S5 N56 1985)
- Stresses in Plates and Shells, A. Ugural, McGraw Hill, 1999. ( TA660.P6 U39 1999)
- Analysis of Shells and Plates, P.L. Gould, Springer-Verlag, 1988, (TA660.S5 G644 1988)
- Structural mechanics: the behavior of plates and shells, J. R. Vinson, Wiley, New York, 1974, ( TA660.P6 V55 1974)
- The Buckling of Plates and Shells, H.L. Cox, Macmillan, NY, 1962 (TA460 .C6x)
- Introduction to the Theory of Shells, C.L. Dym, Hampshire Publishing Corp., 1990. (QA935 .D89 1990)
- The Behavior of Thin Walled Structures: Beams, Plates and Shells, J.R. Vinson, Dordrecht, Netherlands ; Boston Kluwer Academic Publishers, 1989 (TA660.T5 V56 1989).

## Lecture 1:

### Introduction to Plate Bending Problems

#### Introduction

A plate is a planer structure with a **very small thickness** in comparison to the planer dimensions. The forces applied on a plate are perpendicular to the plane of the plate. Therefore, plate resists the applied load by means of **bending** in two directions and **twisting moment**. A plate theory takes advantage of this disparity in length scale to reduce the full three-dimensional solid mechanics problem to a two dimensional problem.

**The aim of plate theory** is to calculate the deformation and stresses in a plate Subjected to loads. A flat plate, like a straight beam carries lateral load by bending. The analyses of plates are categorized into two types based on thickness to breadth ratio:

1. thick plate
2. thin plate analysis.

If the thickness to width ratio of the plate is less than 0.1 and the maximum deflection is less than one tenth of thickness, then the plate is classified as thin plate. **The well known as Kirchhoff plate theory is used for the analysis of such thin plates**. On the other hand, **Mindlin plate theory is used for thick plate where the effect of shear deformation is included**.

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

Theory of plates & shells:-

I - Plates & Theory of plates:-

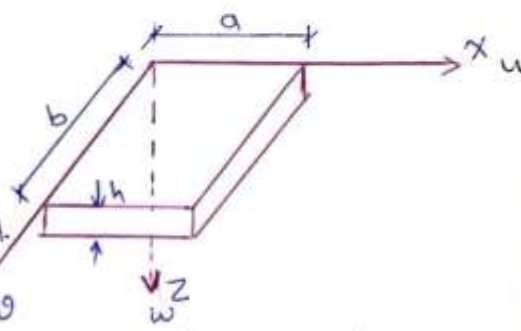
- 1- Thin plate with small defl.
- 2- " " " Large "
- 3- Thick plate

Assuming that  $b < a$

$\therefore$  if  $h \ll \frac{b}{20} \Rightarrow$  thin plates

$w < h \Rightarrow$  Thin plate with small defl.

$w \geq h \Rightarrow$  Thin Plate with Large " y "



$u =$  defl. in x-dir.

$v =$  defl. in y-dir.

$w =$  defl. in z-dir.

- If both conditions are not satisfied it will become thick plate

\* في حالة الـ thin plate حيث ان  $h \ll \frac{b}{20}$  يكون ميل السطح العمودي  $b$  كبيراً جداً مقارنة بسمك  $h$  لذلك يمكن تجاهل تأثيرات انحناء السطح العمودي في تحليل الإجهاد والخصائص الميكانيكية.  
 الـ Thick plate يكون له ميل كبير للسطح العمودي مقارنة بسمك  $h$  لذلك لا يمكن تجاهل تأثيرات انحناء السطح العمودي في تحليل الإجهاد والخصائص الميكانيكية.

Thin plate with small defl. go



1.  $w < h$  ( $h \ll \frac{b}{20}$  where  $b < a$ )

2. Theory is based on Kirchhoff's hypotheses, i.e. classical Theory (line  $\perp$  middle surface before deformation will remain  $\perp$  after deformation  $\Rightarrow$  negligible shear deformations)

3. No middle plane strains are created when bent to developable surface

4. very small middle plane strain are created when bent to non-developable surface

5. Bending and membrane actions are not coupled  
 في حالة الـ shells حيث ان  $h$  كبيراً جداً مقارنة بسمك  $h$  لذلك لا يمكن تجاهل تأثيرات انحناء السطح العمودي في تحليل الإجهاد والخصائص الميكانيكية.

$$\epsilon_x = \frac{\partial u}{\partial x} + \frac{w}{r_x}$$

6. Since deformations are small, the strain-displacement relations are linear  
معادلات الشد تظل تتبع العلاقات الخطية وموازنة

7. Equilibrium equations are derived in the undeformed state, hence are linear.  
معادلات التوازن المستمدة من الحالة غير المشدودة، العلاقات الخطية، التوازن

Lagrange المعادلات

Note This Theory will not give satisfactory stress in case of plates with holes and highly concentrated loads as shear effects are predominating in those cases  
هذه النظرية لن توفر إجهادات مرضية في حالات الثقوب والأحمال المركزة بشدة حيث تكون تأثيرات القص هي المسيطرة في تلك الحالات. ~~Concentrated stress~~ والتأثير غير ذي أهمية.

Thin Plate with Large deflection

1-  $w \gg h$  ( $h \ll \frac{b}{20}$ ,  $b < a$ )  
عندما يكون الانحناء كبيراً بحيث يفوق سمك اللوح، حيث  $h \ll \frac{b}{20}$  و  $b < a$  شرط التواء اللوح

2. Theory is again based on Kirchhoff's hypothesis

3. No middle plane strains are created when bent to a developable surface

4. Middle plane strains are created when bent to a non-developable surface  
(مثل انحناء اللوح على شكل كرة أو سطح غير قابل للتطوير) حيث يتم إنشاء إجهادات في المستوى الأوسط للوح.  
(membrane)

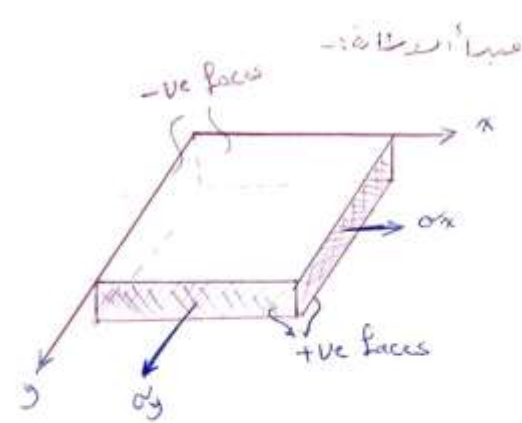
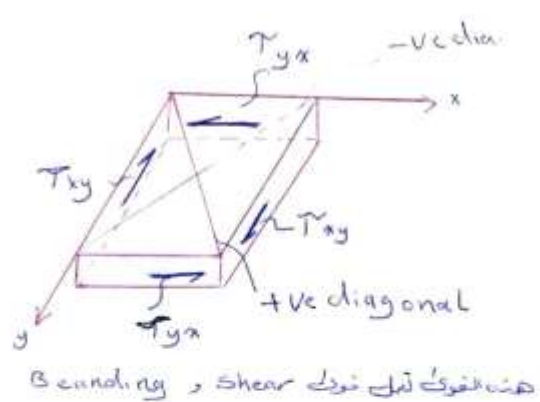
5. Bending and membrane actions are coupled

6. Since deflections are not small (geometrical non-linearity) strain-displacement relations are non-linear

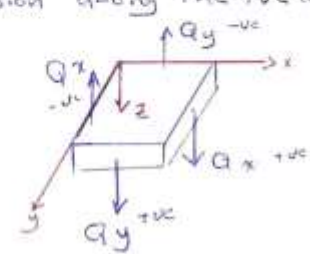
7. Equilibrium equations are derived in the deformed state and hence are non-linear  
معادلات التوازن المستمدة من الحالة المشدودة، العلاقات غير الخطية، التوازن

\* Karman - developed this theory (في صياغة معادلات التوازن)





Shear stress +ve if they produce tension along the +ve diagonal  
 Forces are:- moments  $M_x$  &  $M_y$   
 Twisting mom.  $M_{xy}$  &  $M_{yx}$   
 shear forces  $Q_x$  &  $Q_y$   
 +ve if in direction of +ve Z



### Differential Equation of plate

Shape of the plate is adequately by describing the geometry of its middle surface, which is a surface that bisects the plate thickness (h) at each point

Assumptions:-

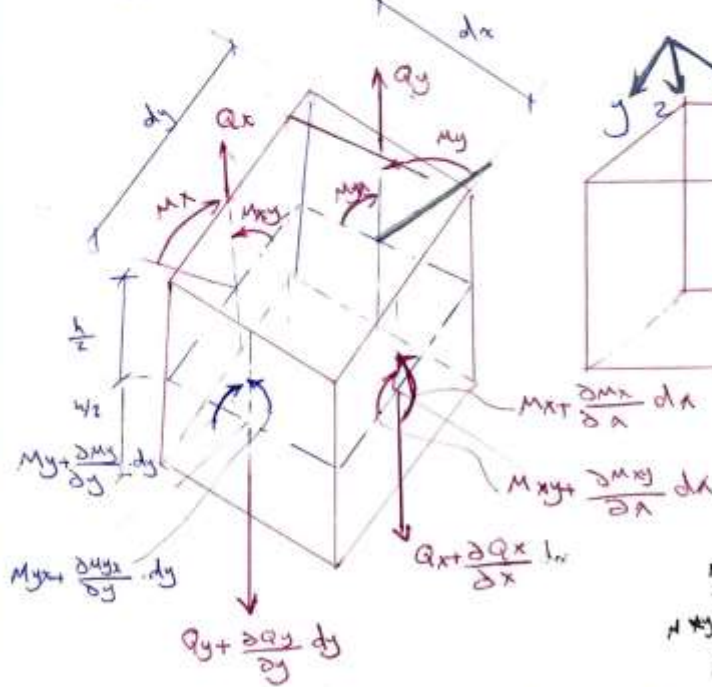
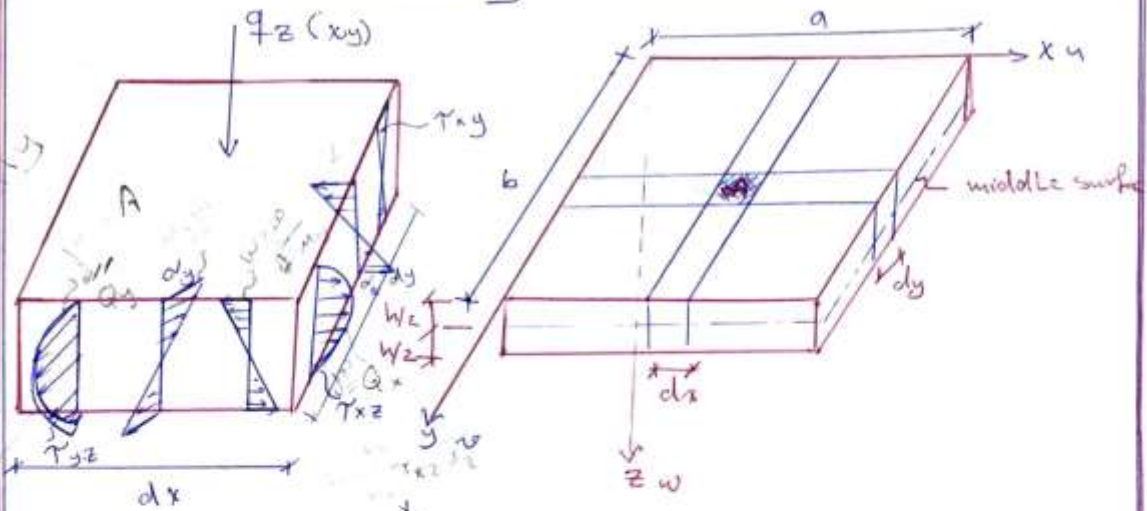
- 1- The material of the plate is elastic homogeneous and isotropic
- 2- The plate is initially flat
- 3- The thickness (h) is small compared to other dimensions
- 4- The deflections are small compared to plate thickness
- 5- The deformations are such that a straight-line initially  $\perp$  to middle surface remain straight line  $\perp$  after deformation.

shear stress distribution

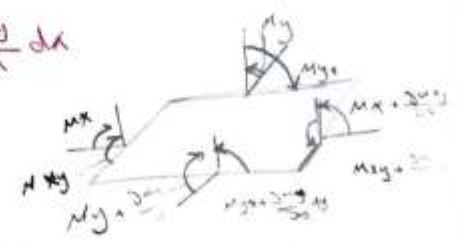
6. The stress  $\perp$  to middle surface are of negligible order of magnitude

« ولست يعطيك ربك فترغب »  
 principle of superposition

The strains in the middle surface produced by inplane forces can usually be neglected in comparison with the strains due to bending.



\* تسمى هذه القوى  
 تسمى القوى من  
 الطبقات الكلت  
 عموماً  $\frac{\partial Q_x}{\partial x}$  كمرمود  
 المسألة  $\frac{\partial Q_y}{\partial y}$  في ذلك  
 حيث كلت الحركه

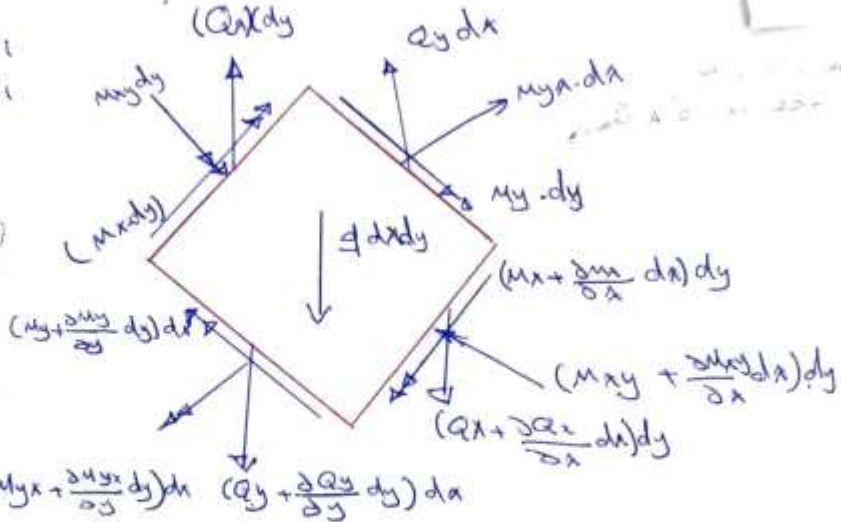


Note: All the action (shear force & bending moment) are per unit length of the middle surface.

معتمد على التفاضل الجزئي

التي هي نتيجة صيغته  
اليه القوت

⊗ اتجاه السكون  
⊙ اتجاه الدوران  
عندما تكون القوى  
موزونة في  
نقطة ما  
فإنها تكون  
موزونة في  
نقطة أخرى



1- Equilibrium in Z direction! -  $\sum F_z = 0$

$$(Q_x + \frac{\partial Q_x}{\partial x} dx) dy - Q_x dy + (Q_y + \frac{\partial Q_y}{\partial y} dy) dx - Q_y dx + q \cdot dx \cdot dy = 0$$

$$\frac{\partial Q_x}{\partial x} + \frac{\partial Q_y}{\partial y} + q = 0 \quad \text{--- ①}$$

2. Moments about y-axis! -

$$(M_x + \frac{\partial M_x}{\partial x} dx) \cdot dy - M_x \cdot dy + (M_{yx} + \frac{\partial M_{yx}}{\partial y} \cdot dy) dx - M_{yx} dx - [(Q_x + \frac{\partial Q_x}{\partial x} dx) dy] \cdot \frac{dx}{2} - (Q_x \cdot dy) \frac{dx}{2} = 0$$

$$\frac{\partial M_x}{\partial x} + \frac{\partial M_{yx}}{\partial y} = Q_x \quad \text{--- ②}$$

Note:- terms with  $(dx)^2$  are eliminated

3. Moment about x-axis! -

$$(M_y + \frac{\partial M_y}{\partial y} dy) dx - M_y \cdot dx + (M_{xy} + \frac{\partial M_{xy}}{\partial x} \cdot dx) dy - M_{xy} \cdot dy - [(Q_y + \frac{\partial Q_y}{\partial y} \cdot dy) dx] \frac{dy}{2} - (Q_y \cdot dx) \frac{dy}{2} = 0$$

$$-\frac{\partial M_y}{\partial y} + \frac{\partial M_{xy}}{\partial x} = -Q_y \quad \text{--- ③}$$

$$\frac{\partial M_{xy}}{\partial x} - \frac{\partial M_y}{\partial y} = -Q_y$$



الآن فنحن نحتاج إلى اشتقاق معادلات المجال بالاشتراك  
 Differentiating eq (2) with respect to (x) and eq (3) with respect to (y) and substituting in eq. (1) we get

$$\frac{\partial^2 M_x}{\partial x^2} + \frac{\partial^2 M_y}{\partial x \partial y} + \frac{\partial^2 M_x}{\partial y \partial x} + \frac{\partial^2 M_y}{\partial y^2} + q = 0$$

observing that  $M_{xy} = M_{yx}$

$$\therefore \frac{\partial^2 M_x}{\partial x^2} + 2 \frac{\partial^2 M_{xy}}{\partial x \partial y} + \frac{\partial^2 M_y}{\partial y^2} + q = 0 \dots (19)$$

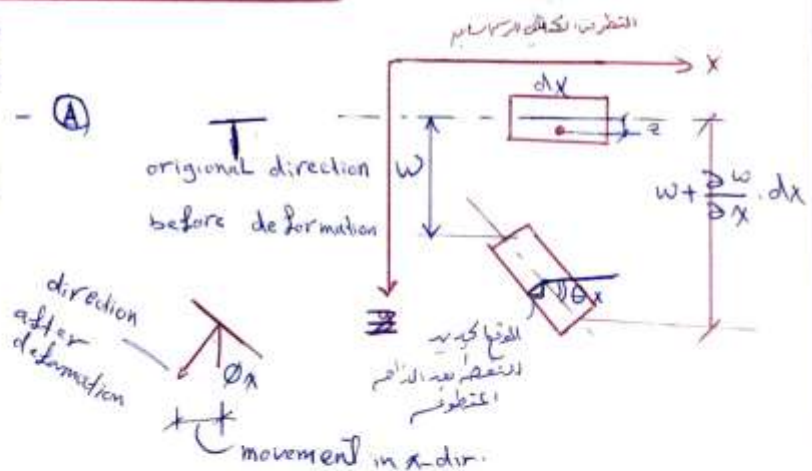
هذا المعادله نحتاج إليها  
 نحتاج إليها لإيجاد  
 deformation

### Compatibility Relations:-

- a) strain - displacement relations
- b. strain - stress "
- c. stress - force "
- d. force - displacement relations

### a. strain - displacement relations:-

$$\left. \begin{aligned} \epsilon_x &= \frac{\partial u}{\partial x} \\ \epsilon_y &= \frac{\partial v}{\partial y} \\ \gamma_{xy} &= \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \end{aligned} \right\} \text{--- (A)}$$



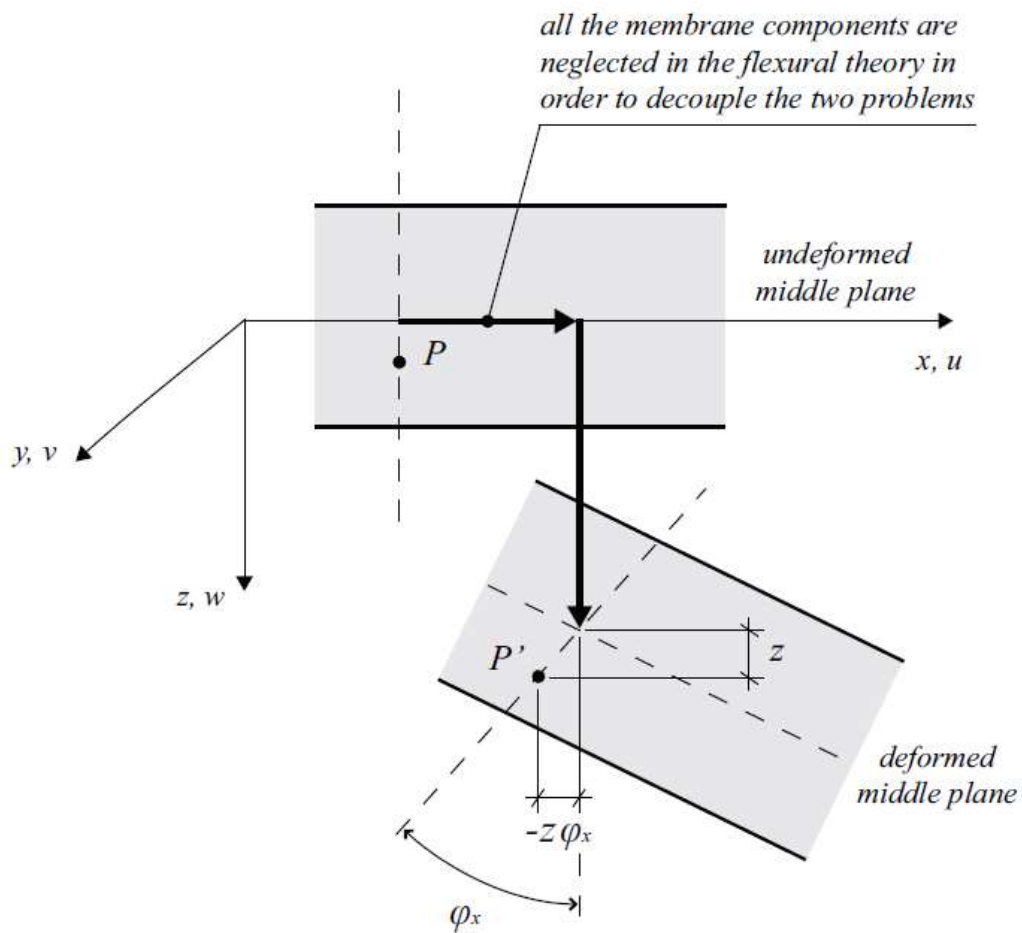


Figure 3: A section of a plate, traced in the  $x$ - $z$  plane, before and after the deformation