

yield Line Analysis of Slabs

Examples

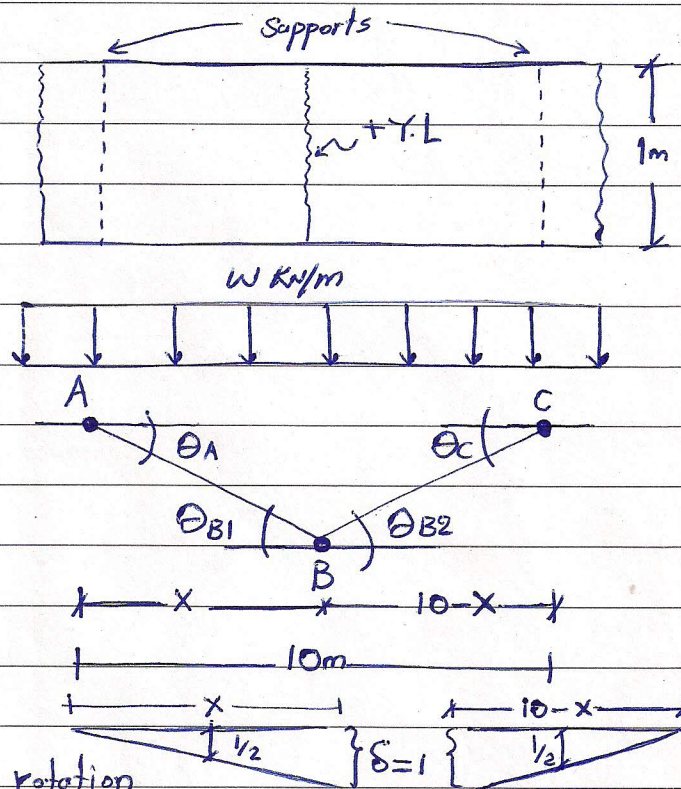
Example-1-

Determine the load Capacity of One-Way Uniformly loaded Continuous slab shown, if $M_{nA} = 25 \text{ Kw}\cdot\text{m/m}$, $M_{nB} = 25 \text{ Kw}\cdot\text{m/m}$ and $M_{nC} = 40 \text{ Kw}\cdot\text{m/m}$

Solution

A unit deflection is given at (B).

External Work done = Load $\times$ area $\times$ (average distance moved for each rigid segment of the slab).

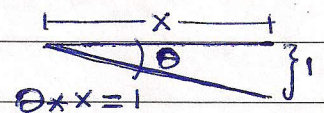


$$W_E = W \times x \times 1 \times \frac{1}{2} + W \times (10-x) \times 1 \times \frac{1}{2}$$

Internal Energy absorbed by rotation along the yield line = Moment $\times$ Length $\times$ Rotation

$$W_I = m \times l \times \theta, \quad \theta_A = \theta_{B1} = \frac{1}{x}$$

$$\text{Also, } \theta_C = \theta_{B2} = \frac{1}{10-x}$$



$$\therefore W_I = M_A \times 1 \times \frac{1}{x} + M_B \times 1 \times \frac{1}{x} + M_B \times 1 \times \frac{1}{10-x} + M_C \times 1 \times \frac{1}{10-x}$$

$$W_E = W_I$$

$$\frac{Wx}{2} + \frac{W(10-x)}{2} = \frac{25}{x} + \frac{25}{x} + \frac{25}{10-x} + \frac{40}{10-x}$$

$$\therefore W = \frac{10}{x} + \frac{13}{10-x}$$

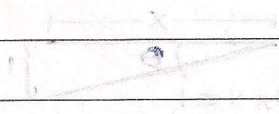
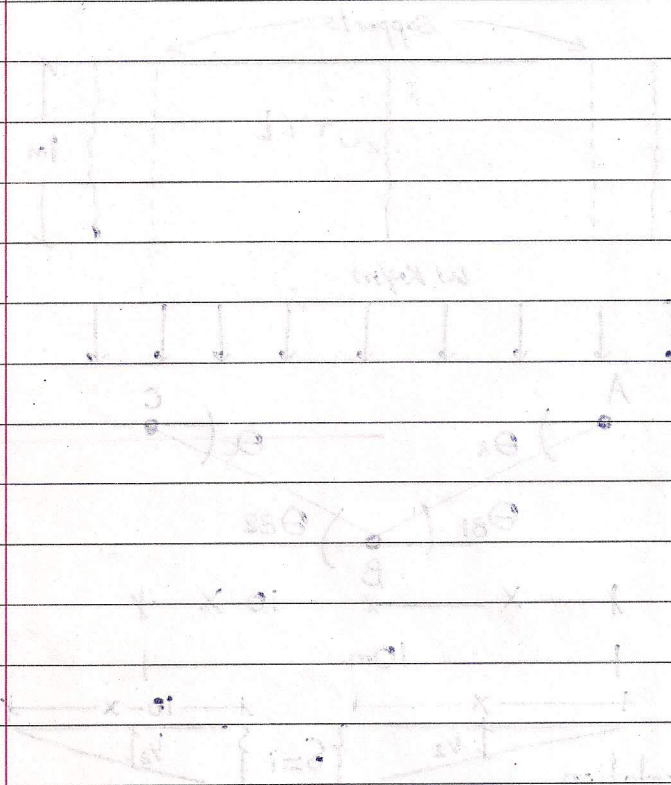
$$\text{To determine minimum } W \Rightarrow \frac{dW}{dx} = 0 = -\frac{10}{x^2} + \frac{13}{(10-x)^2}$$

$$\therefore x = 4.67 \text{ m}$$

Sub $x = 4.67\text{m} \rightarrow W = \frac{10}{4.67} + \frac{13}{10-4.67} = 4.58 \text{ kN/m}^2$

Note

Answer



$$\sum F_x = 0 \Rightarrow R_B - 10x - W(x) = 0$$

$$\sum M = 0 \Rightarrow R_B \cdot x - 10 \cdot \frac{x^2}{2} - W \cdot \frac{x^2}{2} = 0$$

$$W = \frac{10}{x} + \frac{13}{10-x}$$

$$\frac{dW}{dx} = -\frac{10}{x^2} + \frac{13}{(10-x)^2} = 0$$



Example ②

Find collapse load (w) for the square slab of length (L) shown, if the resisting moment in every direction $= m$ kN·m/m (Isotropic slab).

Solution/

$$EW = W \times \left(\frac{1}{2} \times L \times \frac{L}{2} \right) \times \frac{1}{3} \times 4$$

$$= \frac{WL^2}{3}$$

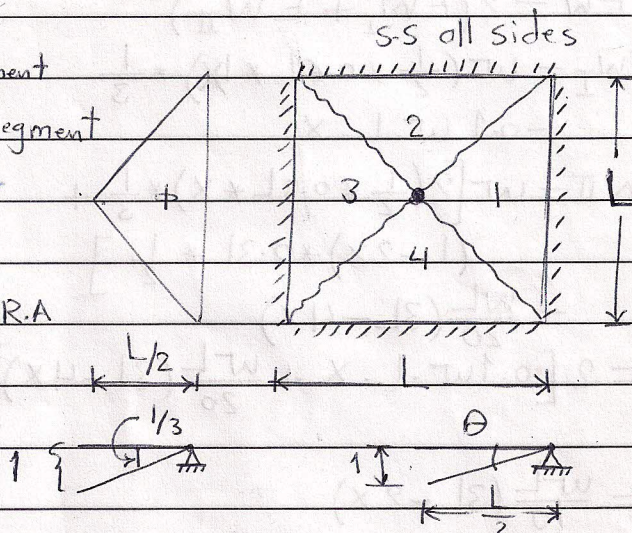
$$IW = m \times \theta \times l$$

projection of Y.L on R.A

$$= m \times \frac{1}{\frac{L}{2}} \times L \times 4 = 8m$$

$$EW = IW$$

$$\frac{WL^2}{3} = 8m \rightarrow W = \frac{24m}{L^2} \quad \text{Answer.}$$



Example ③ For Ex ②, if the slab has the same dimension & boundary conditions, find collapse concentrated force (K) at center of slab.

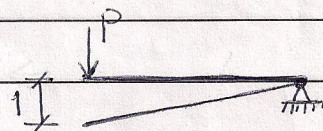
Solution/

$$EW = P \times 1 = P$$

$$IW = 8m \quad (\text{as before})$$

$$EW = IW$$

$$P = 8m \quad \text{Answer.}$$



Example ④ For Ex ②, if the slab is fixed at all sides, find collapse load w , consider $m^+ = m^- = m$

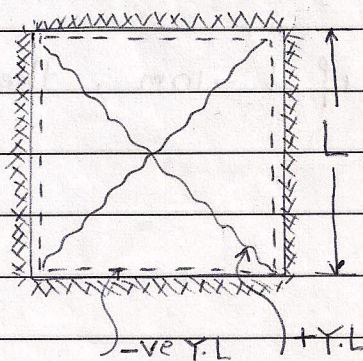
Solution/

$$EW = \frac{WL^2}{3} \quad (\text{as before})$$

$$IW = m^+ \times \frac{1}{L/2} \times L \times 4 + m^- \times \frac{1}{L/2} \times L \times 4 = 16m$$

$$EW = IW \rightarrow \frac{WL^2}{3} = 16m \rightarrow W = \frac{48m}{L^2}$$

Answer





Example ⑥/. Find collapse load w for the S.S rectangular slab shown, assume ultimate moment of resistance in each direction is " m_p ".

Solution/

$$E_w = 2(EW_I + EW_{II})$$

$$EW_I = w \left(\frac{1}{2} \times 0.6L \times x \right) \times \frac{1}{3} = 0.1 w \cdot L \cdot x$$

$$EW_{II} = w \left[2 \left(\frac{1}{2} \times 0.3L \times x \right) \times \frac{1}{3} + (L - 2x) \times 0.3L \times \frac{1}{2} \right] = \frac{wL}{20} (3L - 4x)$$

$$\therefore E_w = 2 \left[0.1 w \cdot L \cdot x + \frac{wL}{20} (3L - 4x) \right] \quad \text{Note/ the segment (II) is divided to two triangles + one rectangle}$$

$$= \frac{wL}{10} (3L - 2x)$$

$$I_w = \left[m_p \times 0.6L \times \frac{1}{x} + m_p \times L \times \frac{1}{0.3L} \right] \times 2 = \left(\frac{3.6L + 20x}{3x} \right) m_p$$

$$E_w = I_w \Rightarrow \frac{wL}{10} (3L - 2x) = \left(\frac{3.6L + 20x}{3x} \right) m_p$$

$$\Rightarrow w = \frac{10}{L} \left[\frac{3.6L + 20x}{3x(3L - 2x)} \right] \Leftrightarrow \text{Rational function } \frac{A}{B}$$

$\frac{BA^2 - AB^2}{B^3}$

for minimum load, $\frac{dw}{dx} = 0$

$$= \frac{60x(3L - 2x) - (3.6L + 20x)(9L - 12x)}{[3x(3L - 2x)]^2}$$

$$120x^2 + 43.2Lx - 32.4L^2 = 0 \rightarrow x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

if $L = 10m$, then $x = 3.7m$ and $w = 0.438 m_p$ $x = 0.37L$

Answer

Example - 7

For the slab shown;
Find $W_{\text{allowable}}$ if $m_p^+ = 20 \text{ kN}\cdot\text{m/m}$, $m_p^- = 25 \text{ kN}\cdot\text{m/m}$
 $l = 6 \text{ m}$

Solution

$$W_E = 3 \left(\frac{1}{2} \times l \times \frac{l}{2\sqrt{3}} \right) \times W \times \frac{1}{3} = \frac{Wl^2}{4\sqrt{3}}$$

$$W_I = 3 \left[(m_p^+ \times l \times \frac{1}{l/2\sqrt{3}}) + (m_p^- \times l \times \frac{1}{l/2\sqrt{3}}) \right]$$

$$= 3 \left[(20 \times 6 \times \frac{2\sqrt{3}}{6}) + (25 \times 6 \times \frac{2\sqrt{3}}{6}) \right]$$

$$= 3 \times 90 \sqrt{3} = 90 (3)^{1.5}$$

$$W_E = W_I \Rightarrow \frac{W \times (6)^2}{4\sqrt{3}} = 90 (3)^{1.5}$$

$$\therefore W = 90 \text{ kN/m}$$

(Note) $\leftrightarrow$ $\frac{1}{2} \times \frac{1}{2}$

W_I can be calculated by using procedure of page (4)
(Rotation about inclined axis)

$$W_I = m^+ \times l \times \frac{1}{\frac{l}{2\sqrt{3}}} + m^- \times l \times \frac{1}{\frac{l}{2\sqrt{3}}}$$

$$= m^+ \times 2\sqrt{3} + m^- \times 2\sqrt{3}$$

$$W_I = m^+ \times l_x \times \frac{1}{dy} + m^+ \times l_y \times \frac{1}{dx} + m^- \times l_x \times \frac{1}{dy} + m^- \times l_y \times \frac{1}{dx}$$

$$= m^+ \times \frac{l}{2} \times \frac{1}{\frac{l}{\sqrt{3}}} + m^+ \times \frac{\sqrt{3}}{2} l \times \frac{1}{\frac{l}{3}}$$

$$+ m^- \times \frac{l}{2} \times \frac{1}{\frac{l}{\sqrt{3}}} + m^- \times \frac{\sqrt{3}}{2} l \times \frac{1}{\frac{l}{3}}$$

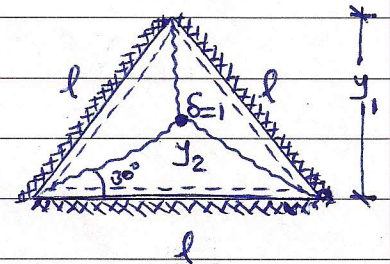
$$= m^+ \left(\frac{\sqrt{3}}{2} + \frac{3\sqrt{3}}{2} \right) + m^- \left(\frac{\sqrt{3}}{2} + \frac{3\sqrt{3}}{2} \right)$$

$$= m^+ \times 2\sqrt{3} + m^- \times 2\sqrt{3}$$

$$W_I = W_I$$

(3)

(2)



$$\tan 60 = y_1 / l/2$$

$$\therefore y_1 = \frac{\sqrt{3} l}{2}$$

$$\tan 30 = y_2 / l/2$$

$$\therefore y_2 = \frac{l}{2\sqrt{3}}$$



$$y_1 = \frac{\sqrt{3}}{2} l \quad y_2 = \frac{l}{2\sqrt{3}}$$

$$dy = y_1 - y_2 = \frac{l}{\sqrt{3}}$$

$$\frac{dx}{dy} = \frac{l/2}{y_1} \Rightarrow dx = \frac{l}{3}$$

YL
5

Class

$$\begin{aligned}
 W_{I \text{ Total}} &= W_{I1} + W_{I2} + W_{I3} = [m^+ \times 2\sqrt{3} + m^- \times 2\sqrt{3}] \times 2 + m^+ \times 2\sqrt{3} + m^- \times 2\sqrt{3} \\
 &= m^+ \times 6\sqrt{3} + m^- \times 6\sqrt{3} \\
 &= 20 \times 6\sqrt{3} + 25 \times 6\sqrt{3} = 270\sqrt{3} \\
 &= 90 \times 3 \times \sqrt{3} = 90 \times (3)^{1.5}
 \end{aligned}$$

↑ As before

OK

Example (8)

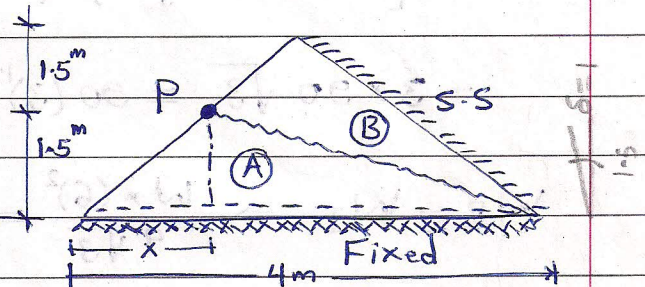
Find Collapse Force (P) for the isotropic triangular slab shown

Assume $m_p^- = m_p^+ = m_p$

Solution

Segment (B) Rotate about inclined axis

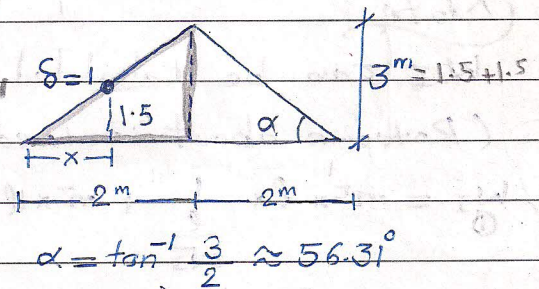
$$W_E = P \times 1 = P$$



$$\begin{aligned}
 W_{I(A)} &= m^+ \times 3 \times \frac{1}{1.5} + m^- \times 4 \times \frac{1}{1.5} \\
 &= \frac{14}{3} m
 \end{aligned}$$

$$\frac{x}{1.5} = \frac{2}{3} \Rightarrow x = 1m$$

$$\begin{aligned}
 W_{I(B)} &= m^+ \times l_x \times \frac{1}{dy} + m^+ \times l_y \times \frac{1}{dx} \\
 &= m \times 3 \times \frac{1}{3} + m \times 1.5 \times \frac{1}{2} \\
 &= 1.75 m
 \end{aligned}$$



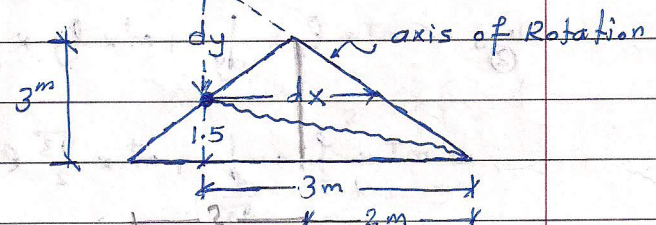
$$\alpha = \tan^{-1} \frac{3}{2} \approx 56.31^\circ$$

$$W_{I \text{ Total}} = \frac{14}{3} m + 1.75 m = 6.417 m$$

$$W_E = W_I$$

$$P = 6.417 m_p$$

Answer



$$\frac{3}{2} = \frac{1.5 + dy}{3}$$

$$dy = \frac{9}{2} - 1.5 = 3m$$

$$\begin{aligned}
 \frac{3}{dx} &= \frac{dy + 1.5}{3} \\
 dx &= 2m
 \end{aligned}$$

Example ⑨

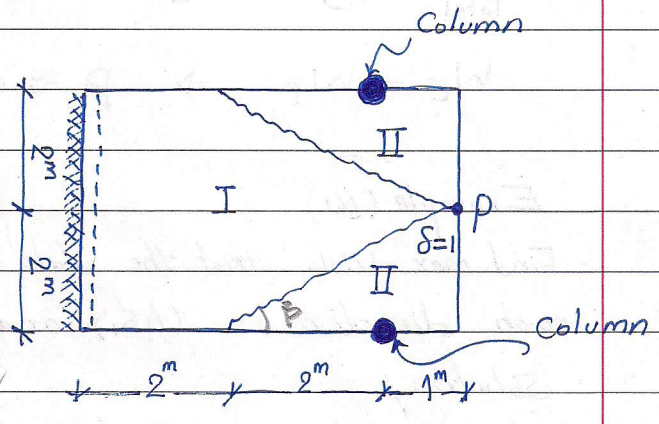
Find $P_{collapse}$ $m_p^+ = m_p^- = m_p$

Solution

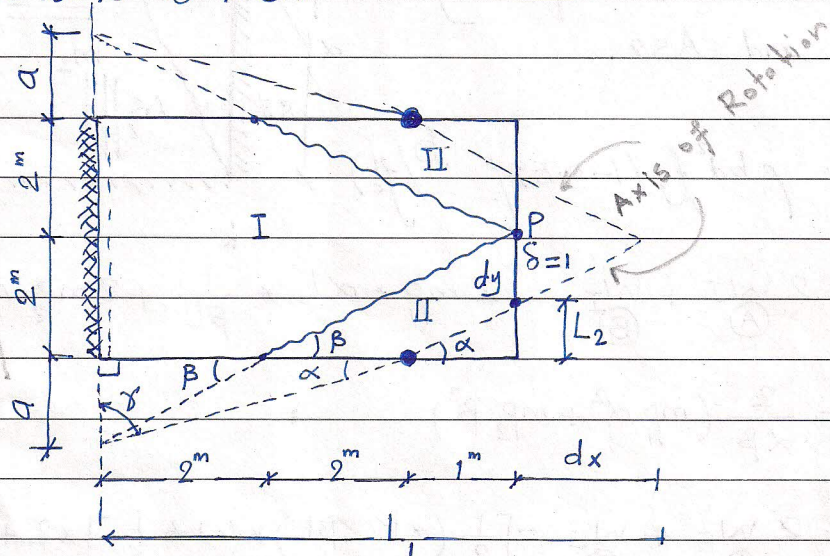
$$\beta = \tan^{-1} \frac{2}{3} \approx 33.7^\circ$$

$$\tan \beta = \frac{a}{2} \Rightarrow a = \frac{4}{3}$$

$$\alpha = \tan^{-1} \frac{a}{4} = \tan^{-1} \frac{4/3}{4} \approx 18.43^\circ$$



$$\gamma = 90 - \alpha = 90 - 18.43^\circ \approx 71.57^\circ$$



$$\tan \gamma = \frac{L_1}{2+a} \Rightarrow L_1 = (2+a) * \tan \gamma$$
$$= (2 + \frac{4}{3}) * \tan 71.57 = 10 \text{ m} \checkmark$$
$$\therefore dx = 10 - (2+2+1) = 5 \text{ m} \leftarrow$$

$$L_2 = \tan \alpha \times 1 = \tan(18.43) \times 1 = 0.33 \text{ m}$$

$$\therefore dy = 2 - L_2 = 2 - 0.33 = 1.67 \text{ m} \leftarrow$$

$$W_E = p \cdot 1 = p$$

$$\textcircled{I} \quad WI = mp^+ * 4 * \frac{1}{5} + mp^- * 4 * \frac{1}{5} = \frac{8}{5} mp$$

$$\textcircled{\text{II}} \quad W_I = m p^+ * l_x * \frac{1}{d_y} + m p^+ * l_y * \frac{1}{d_x}$$

$$= mp * 3 * \frac{1}{1.67} + mp * 2 * \frac{1}{5} = 2.2 mp$$

Two squints

$$W_{I \text{ Total}} = W_{I \text{ (I)}} + 2 W_{I \text{ (II)}} = \left(\frac{8}{5} + 2 \times 2.2 \right) m_p \approx 6 m_p$$

$$W_E = W_I \Rightarrow p \approx 6 m_p$$

Answer

Example (10)

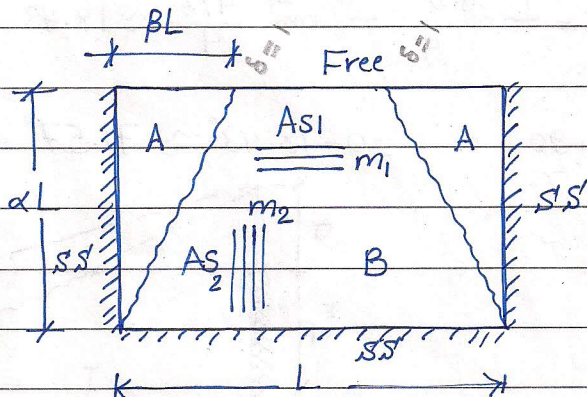
Find max. UDL that the slab can sustain if its reinforcement in each direction is (AS_1) and (AS_2) as shown.

Solution /

Let m_{p1} and m_{p2} the moment of resistance corresponding to AS_1 and AS_2

Note

$$m_p = \rho b d^2 f_y (1 - 0.59 \rho f_y / f_c)$$



$$W_I = 2 W_{I \text{ (A)}} + W_{I \text{ (B)}} = 2 m_{p1} \times \alpha L \times \frac{1}{\beta L} + 2 m_{p2} \times \beta L \times \frac{1}{\alpha L}$$

$$= \frac{2}{\alpha \beta} (m_{p1} \alpha^2 + m_{p2} \beta^2)$$

$$W_E = 2 W_{E \text{ (A)}} + W_{E \text{ (B)}} = \left[\frac{1}{2} (\alpha L - \beta L) \times w \times \frac{1}{3} \right] \times 2 + 2 \left[\frac{1}{6} w \alpha \beta L^2 + \alpha L \left(\frac{L}{2} - \beta L \right) w \times \frac{1}{2} \right]$$

$$= \frac{1}{6} \alpha (3 - 2\beta) L^2 \times w$$

$$W_E = W_I \Rightarrow w = \frac{\frac{2}{\alpha \beta} (m_{p1} \alpha^2 + m_{p2} \beta^2)}{\frac{\alpha}{6} (3 - 2\beta) L^2} = \frac{12 (m_{p1} \alpha^2 + m_{p2} \beta^2)}{\alpha^2 L^2 (3\beta - 2\beta^2)}$$

It varied according to β .

$$\text{Let } m_{p2} = \mu m_{p1}$$

أي أن النسبة بين العزمين μ

$$\therefore w = \frac{12 m_{p1} (\alpha^2 + \mu \beta^2)}{\alpha^2 L^2 (3\beta - 2\beta^2)}$$