

Second Class /Materials Engineering Department

Torsion(twisting)

Derivation of Torsion Formula

In deriving the torsion formulas , we make the following assumptions. The first two apply only to shaft of circular section:

1. Circular section remain circular.
2. Plane section remain plane and don't warp.
3. The projection upon a transverse section of straight radial line in the section remains straight. As show fig.2
4. Shaft is loaded by twisting couples(**torque**) in planes that are perpendicular to the axis of the shaft.
5. Stresses don't exceed the proportional limit.

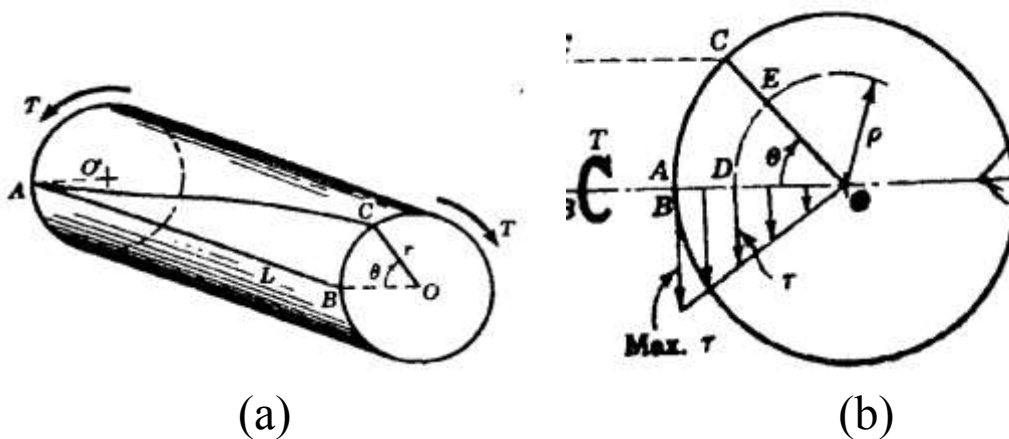


Fig.1

The total shearing deformation δ_s , as shown in fig.1 is given by:

$$\delta_s = DE = \rho\theta \text{ -----(a)}$$

where:

DE is the arc length of a circle whose radius ρ

ρ is a circle radius

θ is the twisted angle in radian (not degree)

((to express θ in degree multiply by $180/\pi = 57.3 \text{ deg/ rad}$))

The unit deformation of this fiber(called Shear strain) is

$$\gamma = \delta_s / L = \rho\theta / L \text{ -----(b)}$$

the shearing stress is determined from Hooke's law:

$$\tau = G \gamma = (G\theta/L)\rho \text{ -----(c)}$$

where

τ is shear stress

G is modulus of rigidity for shaft materials.

Now , a differential area of section M-N at a radial distance ρ from the axis of the shaft carries the differential load , as show fig.2

$$dP = \tau dA.$$

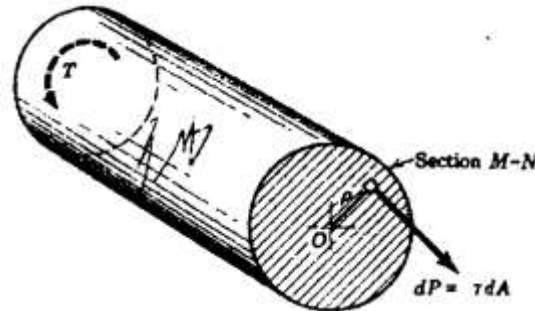


Fig.2

The fact that applied torque T equal the resisting torque T_r , where T_r is the sum of resisting torque developed by all differential loads dP .

$$T = T_r = \int \rho dP = \int \rho (\tau dA)$$

Replacing by its valus from eq. (c) gives

$$T = (G\theta/L) \int \rho^2 dA$$

$$\text{Since } \int \rho^2 dA = J$$

Where

J is the polar moment of inertia of cross section.

$$T = G \theta J/L$$

Then

$$\theta = TL/GJ \quad \text{-----(1)}$$

by replacing the product $G\theta/L$ in eq.(c) by T/J

we obtain

$$\tau = T\rho/J \quad \text{-----(2)}$$

But, the maximum shearing stress is obtained at surface of shaft then replaced ρ by r radius of shaft.

$$\text{Max. } \tau = Tr/J \quad \text{-----}(2a)$$

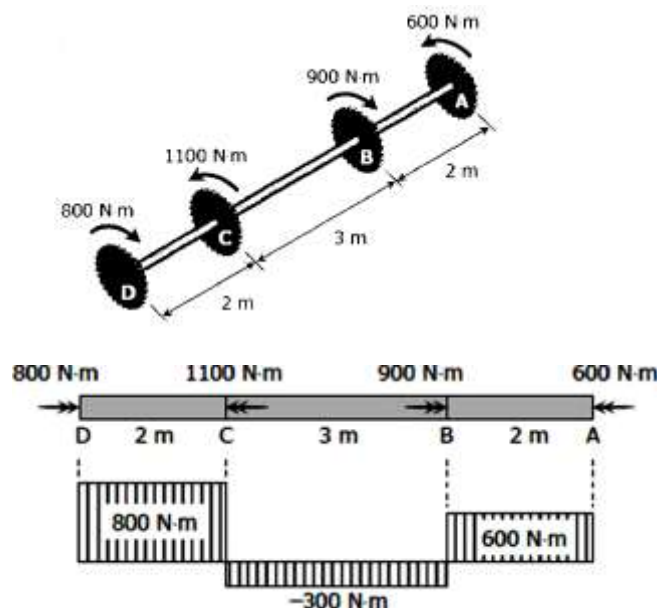
When J value is applied in eq.2a , we obtained:

$$\text{Solid shaft:} \quad \text{Max. } \tau = \frac{2T}{\pi r^3} = \frac{16T}{\pi d^3}$$

$$\text{Hollow shaft:} \quad \text{Max. } \tau = \frac{2TR}{\pi(R^4 - r^4)} = \frac{16TD}{\pi(D^4 - d^4)}$$

Ex/ An aluminum shaft with a constant diameter of 50 mm is loaded by torques applied to gears attached to it as shown in fig below. Using $G = 28 \text{ GPa}$, determine the shearing stress for each segment and the relative angle of twist of gear D relative to gear A.

(Note/ review question 210 in the book , you can see the similarity of solution method between two questions)



$$\tau_{max} = \frac{16T}{\pi d^3}$$

$$\tau_{max_{A-B}} = \frac{16T}{\pi d^3}$$

$$= 16 \times 600 \text{ N.m} / \pi (50\text{mm})^3 = 9600 \text{ N.m} / \pi 12500 \times 10^{-6}\text{m} = ?$$

$$\tau_{max_{B-C}} = \frac{16T}{\pi d^3}$$

$$= 16 \times 300\text{N.m} / \pi (50\text{mm})^3 = 4800 \text{ N.m} / \pi 12500 \times 10^{-6}\text{m} = ?$$

$$\tau_{max_{C-D}} = \frac{16T}{\pi d^3}$$

$$= 16 \times 800\text{N.m} / \pi (50\text{mm})^3 = 12800 \text{ N.m} / \pi 12500 \times 10^{-6}\text{mm} = ?$$

$$\theta = \frac{TL}{JG}$$

Rotation of D relative to A:

$$\theta_{D/A} = \frac{1}{JG} \sum TL$$

$$\theta_{D/A} = \frac{1}{\frac{1}{32} \pi (50^4) (28\,000)} [800(2) - 300(3) + 600(2)] (1000^2)$$

$$\theta_{D/A} = 0.1106 \text{ rad} \times 57.3 \text{ deg/rad}$$

$$\theta_{D/A} = ? \text{ }^\circ$$