

A **viscous material** is one that is **semi-fluid in nature**. When **stressed**, it will **deform** or tend to deform, any **deformation** being **permanent** because it is not **recovered** when the loading is **removed**.

**Elastic materials** also **deform** or tend to deform when **stressed**, but, when the **loading is removed**, any deformation is **fully recovered**.

**Bitumens** are **visco-elastic materials**. The degree to which their behavior is **viscous and elastic** is a **function of both temperature and the period of loading** (usually referred to as the '**loading time**').

At **high temperatures** or **long loading times** they behave as **viscous liquids**, whereas at **very low temperatures** or **short loading times** they **behave as elastic (brittle) solids**.

**The intermediate range of temperature and loading times**, more typical of conditions in service, results in **visco-elastic behavior**.

In order to define the **visco-elastic** properties, the **concept of the stiffness modulus** as a **fundamental parameter** to describe the mechanical properties of bitumens by analogy to the **elastic modulus** of **solids** was introduced.

If a **tensile stress  $s$**  is applied at a loading time  **$t = 0$** , a strain  **$\epsilon$**  is instantly attained that **does not increase** with the **loading time**. The elastic modulus  **$E$**  of the material is expressed by **Hooke's law** as **stress divided by strain**.

In the case of **visco-elastic materials** such as **bitumen**, a **tensile stress  $s$**  applied at a loading time  **$t = 0$**  causes a strain  **$\epsilon$**  that **increases**, but **not proportionately**, with the **loading time**. The stiffness modulus  **$S_t$**  at a loading time  **$t$**  is defined as **the ratio between the applied stress and the resulting strain at the loading time  $t$** .

It follows from the above that the value of the **stiffness modulus** is dependent on the **temperature** and the **loading time** that is due to **the special nature of bitumen**.

Consequently, it is necessary to state both the temperature **T** and the loading time **t** of any stiffness modulus measurement

$$S_{t,T} = \frac{\sigma}{\epsilon_{t,T}}$$

The **methods** used to measure the **stiffness modulus of bitumen** are often based on **shear deformations**. The resistance to shear is expressed in terms of the **shear modulus G**, which is defined as

$$G = \frac{\text{Shear stress}}{\text{Shear strain}}$$

The **elastic modulus** and **shear modulus** are related by  **$E = 2(1 + \mu)G$**

where  **$\mu$**  is **Poisson's ratio**. The value of  **$\mu$**  depends on the **compressibility** of the material, and may be assumed to be **0.5** for almost **incompressible pure bitumens**, while values of **<0.5** have to be considered for **asphalts**.

Thus,  **$E \sim 3G$**

## Prediction of the stiffness modulus

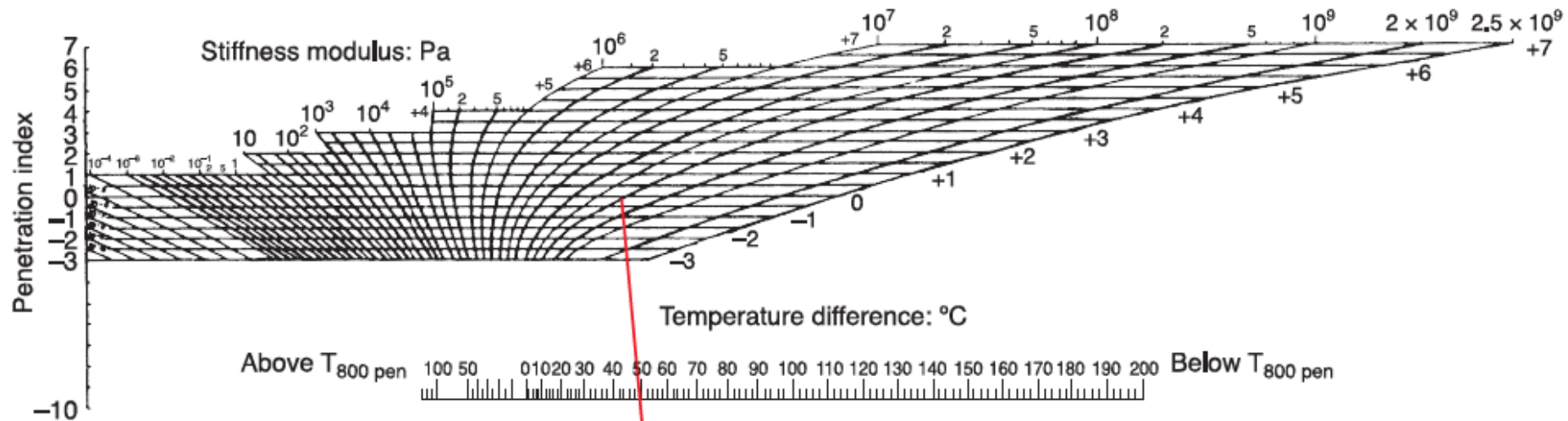
If direct measurement of the stiffness modulus is **not feasible**, it can be predicted using the **Van der Poel nomograph**.

**Van der Poel** showed that two bitumens of the **same PI** at the **same loading time** have **equal stiffness moduli** at **temperatures** that **differ** from their **respective softening points** by the **same amount**.

Over **40 bitumens** were tested with **PI** values varying from **+6.3** to **-2.3** at **many temperatures and frequencies**, using both **creep tests** and **dynamic tests**.

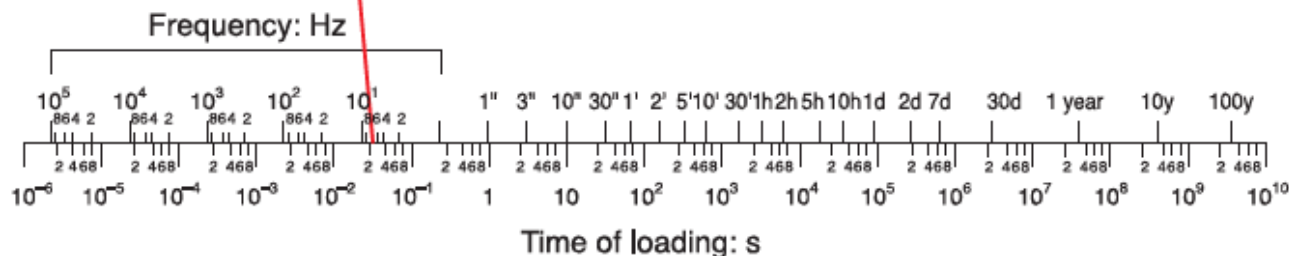
From the test data, **Van der Poel** produced a **nomograph** from which, using only **penetration** and the **softening point**, it is possible to predict the **stiffness modulus** of a bitumen over a wide range of conditions of **temperature and loading times**.

**Figure 6.17** (Shell Handbook, sixth edition 2015) shows a Van der Poel nomograph with the stiffness modulus determined for a **40/60 pen** bitumen at a loading time of **0.02 s** and a test temperature of **58°C**.



To determine the stiffness modulus of a 50 pen bitumen at the test conditions, connect 0.02 s on the loading time-scale with  $(53.5 + 1.5 - 5 = 50^\circ\text{C})$  on the temperature scale. Stiffness modulus is  $1.5 \times 10^8$  Pa at a PI of 0.

Conditions:  
 Loading time – 0.02 s  
 Temperature  $5^\circ\text{C}$   
 Bitumen properties:  
 Penetration at  $25^\circ\text{C}$  – 50 dmm  
 Softening point (IP) –  $53.5^\circ\text{C}$   
 PI – 0.0



**Figure 6.17** Nomogram for determining the stiffness modulus of bitumens

## Example/page 19

For a bitumen with **PI= +2** and  $T_{R\&B}=75^{\circ}\text{C}$ . Determine the stiffness modulus  $S_B$  of the bitumen at test temperature  **$-11^{\circ}\text{C}$**  and frequency of **10 Hz**.

## Solution

- 1) Connect the frequency **10 Hz** represented by Point 1 on the loading time scale with  $T_{\text{difference}}=86^{\circ}\text{C}$  [75-(-11)] represented by point 2 on the temperature scale.
- 2) Extend the line to connect the line drawn from **PI= +2** represented by point 3.
- 3) Mark the resulting intersection point (point 4) on the nomograph.
- 4) Draw a curve line from the conflict point (point 4) parallel to the main curve lines to intersect the stiffness modulus side (point 5).
- 5) Predict the stiffness modulus from point 5,  $S_B = 5 \cdot 10^8 \text{ N/m}^2$ .

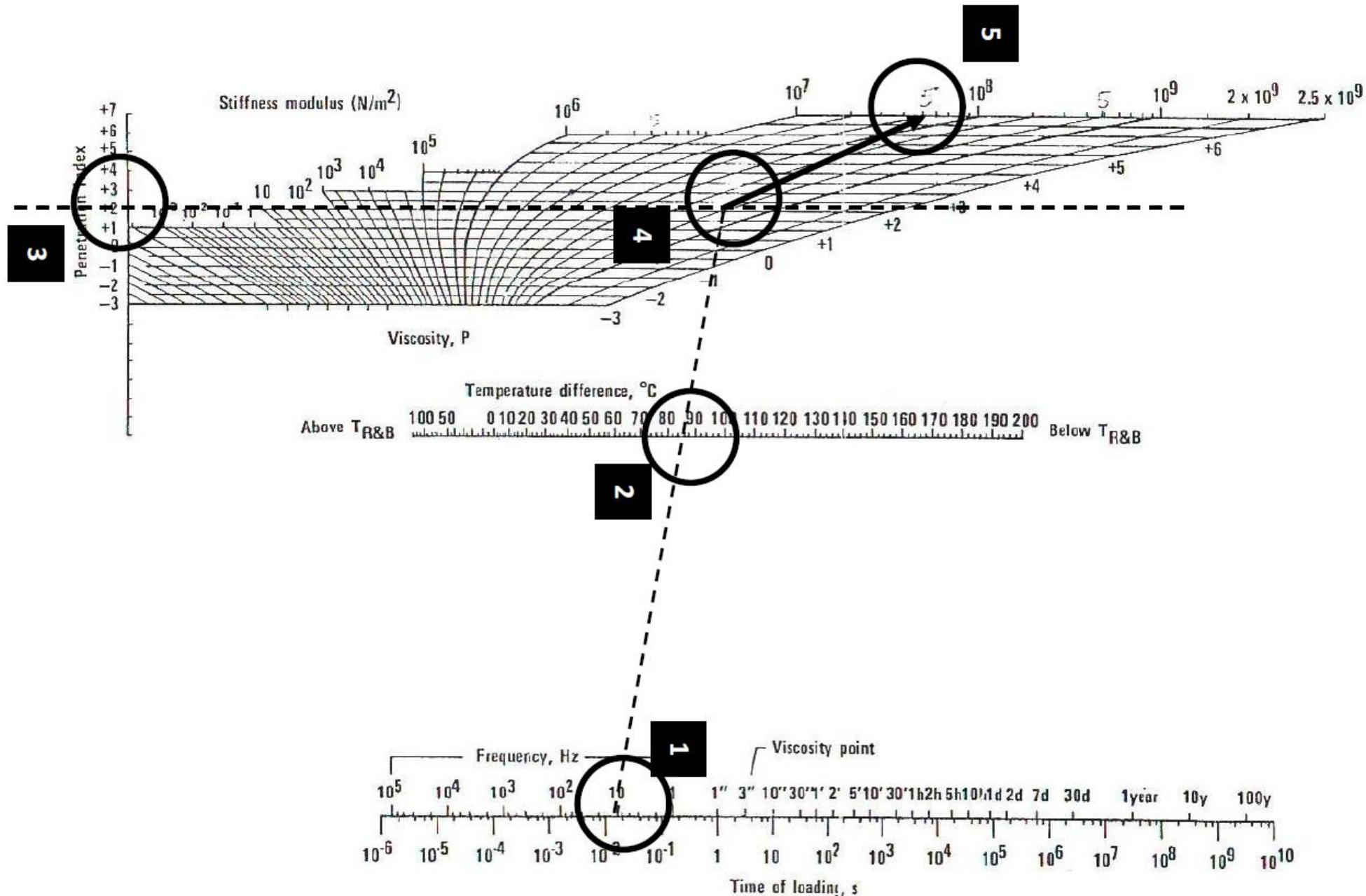


Figure 8.15. KSLA nomograph for  $S_b$  (bitumen stiffness). (From Shell Oil Co.)

Frequency ( $f$ ) is the number of occurrences of a repeating event per unit of time.

Frequency is measured in units of hertz (Hz) which is equal to one occurrence of a repeating event per second. Hz = hertz = 1/s.

Frequency means oscillations (cycles) per second.

### Ex.

$$\text{Hz} = 1/\text{s} = 1/10 = 0.1 \text{ Hz}$$

$$\text{Hz} = 1/\text{s} = 1/2 = 0.5 \text{ Hz}$$

$$\text{Hz} = 1/\text{s} = 1/0.5 = 2.0 \text{ Hz}$$

$$\text{Hz} = 1/\text{s} = 1/1 = 1.0 \text{ Hz}$$

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$$1 \text{ second} = 1 \text{ s} = 1000 \text{ ms}$$

$$1 \text{ ms} = 0.001 \text{ s}$$

$$1 \mu\text{s} = 0.000001 \text{ s}$$

cps = cycles per second