

Chapter-3

Unsteady State Heat Conduction

The general form of heat transfer by conduction is:

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

For one dimension, unsteady state heat conduction with no heat generation ($\dot{q}=0$) \Rightarrow

$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \Rightarrow T = f(x,t) ; \alpha = k/\rho c$$

There are three main types of boundary conditions

1. Constant wall temp.
2. Constant heat flux.
3. Convection boundary condition

Geometries:

1. Lumped heat capacity system.
2. Semi-Infinite solid.
3. Infinite Plate.
4. Infinite cylinder.
5. Short cylinder.
6. Sphere.

Infinite Plate: The differential Eqn is $\frac{d^2 \theta}{dx^2} = \frac{1}{\alpha} \frac{d\theta}{dt} ; \theta = T - T_i$

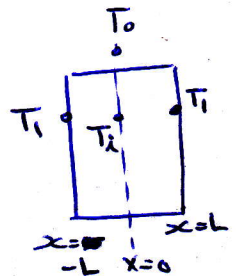
IC. @ $t=0, T=T_i, \theta=\theta_i = T_i - T_i$

BC(1) @ $x=L, \theta=0 ; t>0$

BC(2) @ $x=-L, \theta=0 ; t>0$

The solution is

$$\frac{\theta}{\theta_i} = \frac{T - T_i}{T_i - T_i} = \frac{4}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} e^{-\left[\frac{n\pi}{2L}\right]^2 \alpha t} \cdot \sin \frac{n\pi}{2L} x$$



Lumped Heat Capacity System

The lumped heat capacity method of analysis is used for systems in which a uniform temperature exists, i.e., no temperature gradient is found.

For a hot body immersed in a cool vessel of water, the energy balance is:

$$\text{In} - \text{out} = \text{Acc.}$$

$$0 - hA(T - T_{\infty}) = \rho V c_p \frac{dT}{dt}$$

where A = surface area of convection (m^2)

V = volume of the body (m^3)

ρ = Density of solid (kg/m^3)

c_p = specific heat of the body ($\text{J}/\text{kg}\cdot\text{K}$)

h = convective heat transfer coefficient. ($\text{W}/\text{m}^2\text{K}$) ($\text{J}/\text{s}\cdot\text{m}^2\text{K}$)

$$\frac{dT}{dt} + \frac{hA}{\rho V c_p} (T - T_{\infty}) = 0 \Rightarrow \frac{d\theta}{dt} + \frac{hA}{\rho V c_p} \theta = 0 \quad ; \quad \theta = T - T_{\infty}$$

By integration factor, the solution is: $\theta = C e^{-\left(\frac{hA}{\rho V c_p}\right)t}$

IC @ $t=0$, $T=T_i \Rightarrow \theta = \theta_i$

$$\Rightarrow \theta_i = C$$

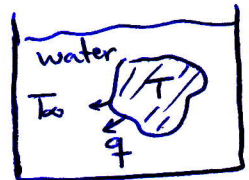
\Rightarrow The solⁿ is

$$\frac{\theta}{\theta_i} = e^{-\left(\frac{hA}{\rho V c_p}\right)t}$$

The expression $\frac{\rho V c_p}{hA}$ has units of time, and is called the time constant of the system (τ).

$$\tau = \text{Resistance} \times \text{capacitance} = \frac{1}{hA} \times \rho V c_p$$

$$\Rightarrow \frac{\theta}{\theta_i} = e^{-\frac{t}{\tau}}$$



Application of lumped heat capacity

The criteria of applying lumped heat capacity for a system is by obtaining the value of Biot number (Bi)

$$Bi = \frac{h(V/A)}{K} \leq 0.1$$

Example: A steel ball ($c_p = 0.46 \text{ kJ/kg}\cdot\text{K}$), $k = 35 \text{ W/m}\cdot\text{K}$), 50mm in diameter and initially at a uniform temp. of 450°C is suddenly placed in a controlled environment in which the temp. is maintained at 100°C . The convection heat transfer coefficient is $10 \text{ W/m}\cdot\text{K}$. Calculate the time required for the ball to attain a temp. of 150°C ($\rho_{\text{steel}} = 7800 \text{ kg/m}^3$).

Solⁿ

$$r = d/2 = 25 \times 10^{-3} \text{ m}$$
$$Bi = \frac{hS}{K} ; S = V/A = \frac{\frac{4}{3}\pi(25 \times 10^{-3})^3}{4\pi(25 \times 10^{-3})^2} = 0.0083$$

$$Bi = \frac{10(0.0083)}{35} = 0.0023 < 0.1 \Rightarrow \text{lumped heat system}$$

$$\tau = \frac{\rho c_p V}{hA} = \frac{(7800)(460) \left(\frac{4}{3}\pi(0.0025)^3\right)}{10 \times 4\pi(0.0025)^2} = 2988 \text{ sec.}$$

$$\theta = \theta_i e^{-t/\tau} ; \theta_i = T_i - T_\infty = 450 - 100 = 350^\circ\text{C}$$

~~$\theta = 150 - 100$~~

$$\theta = T - T_\infty = 150 - 100 = 50^\circ\text{C}$$

$$\Rightarrow 50 = 350 e^{-t/2988} \Rightarrow t = 5818 \text{ sec.} = 1.616 \text{ hr.}$$

Example: Determine the time required for a 1.25 cm diameter steel sphere ($k = 40 \text{ W/mK}$) to cool from $T_i = 500^\circ\text{C}$ to 100°C if exposed to a cooling air flow at $T_\infty = 25^\circ\text{C}$ resulting in $h = 110 \text{ W/m}^2\text{K}$, $\rho_{\text{steel}} = 7801 \text{ kg/m}^3$, $c_p = 473 \text{ KJ/kgK}$.

Soln $Bi = \frac{h(V/A)}{k} = \frac{(110)(0.0125)}{(40)(6)} = 0.0057 < 0.1 \Rightarrow \text{lump}$

$$\frac{\theta}{\theta_i} = \frac{T - T_\infty}{T_i - T_\infty} = e^{-t/\tau} \quad ; \quad \tau = \frac{\rho c_p V}{hA}$$

$$\frac{100 - 25}{500 - 25} = 0.1579 = \text{Exp} \left[\frac{-t}{\frac{(7801)(473)(0.0125)}{(6)(110)}} \right] \Rightarrow t = 2.16 \text{ min}$$

Example For the steel of the above example, determine:

- The instantaneous heat transfer rate 2 min after the start of cooling.
- The total energy transferred from the sphere during the first two minutes.

Soln (a) $q = hA(T - T_\infty) = hA(T_i - T_\infty) e^{-t/\tau}$
 $= 110 * \pi (0.0125)^2 (500 - 25) e^{\left[\frac{-120}{\frac{7801 * 473 * 0.0125}{6 * 110}} \right]}$

$$= 0.405 \text{ W}$$

(b) $Q = \int_0^t q \cdot dt = \int_0^t hA(T_i - T_\infty) e^{-t/\tau} \cdot dt = hA(T_i - T_\infty) \int_0^t e^{-t/\tau} \cdot dt$

$$= -\tau hA(T_i - T_\infty) \cdot e^{-t/\tau} \Big|_0^t = \tau hA(T_i - T_\infty) (1 - e^{-t/\tau})$$

$$= \rho c_p V (T_i - T_\infty) (1 - e^{-t/\tau})$$

$$= 7801 * 473 * \frac{\pi}{6} (0.0125)^3 \left[1 - e^{\left[\frac{-120}{\frac{7801(473)(0.0125)}{6 * 110}} \right]} \right] (500 - 25)$$

$$= 1.467 \text{ kJ}$$

Example: An aluminium sphere weighing 7 kg and initially at a temp. of ~~260~~ 260°C is suddenly immersed in a fluid at 10°C. If $h = 50 \text{ W/m}^2\text{K}$, determine the time required to cool the sphere to 90°C. given $\rho = 2707 \text{ kg/m}^3$, $C_p = 900 \text{ J/kgK}$, $k = 204 \text{ W/mK}$.

Solⁿ

$$V = \frac{\text{mass}}{\rho} = \frac{7 \text{ kg}}{2707 \frac{\text{kg}}{\text{m}^3}} = 2.58 \times 10^{-3} \text{ m}^3$$

$$V = \frac{4}{3} \pi r_0^3 \Rightarrow r_0 = \left(\frac{3V}{4\pi} \right)^{1/3} = \left(\frac{3(2.58 \times 10^{-3})}{4\pi} \right)^{1/3} = 0.085 \text{ m}$$

$$\frac{V}{A} = \frac{r_0}{3} = 0.028 \text{ m}$$

$$Bi = \frac{hr_0}{3k} = \frac{50(0.085)}{3(204)} = 0.007 < 0.1$$

∴ Internal resistance can be neglected.

$$\frac{T - T_\infty}{T_0 - T_\infty} = e^{-t/\tau}$$

$$\tau = \frac{\rho C_p V}{h A} = \frac{(2707)(900)(0.085)}{3(50)} = 1388.89 \text{ sec}$$

$$\frac{90 - 10}{260 - 10} = e^{-t/1388.89} \Rightarrow t = 1580 \text{ sec.}$$

Example: A thermocouple junction, which may be approximated as a sphere, is to be used for temp. measurement in a gas stream. The convection coefficient between the junction surface & the gas is known to be $h = 400 \text{ W/m}^2\text{K}$ and the junction thermophysical properties are $k = 20 \text{ W/mK}$, $c_p = 400 \text{ J/kgK}$, and $\rho = 8500 \text{ kg/m}^3$. Determine the junction diameter needed for the thermocouple to have a time constant of 1 sec. If the junction is at 25°C and is placed in a gas stream that is at 200°C , how long will it take for the junction to reach 199°C ?

Solⁿ Assume lumped heat capacity system

$$\tau = \frac{\rho c_p V}{hA} = \frac{\rho c_p \frac{\pi D^3}{6}}{h \pi D^2}$$

$$\Rightarrow D = \frac{6h\tau}{\rho c_p} = \frac{6 \times 400 \times 1}{8500 \times 400} = 7.06 \times 10^{-4} \text{ m} \rightarrow r = \frac{D}{2}$$

$$\frac{D}{L_c} = \frac{r_0}{L_c} \Rightarrow Bi = \frac{hr_0}{3k} = \frac{400 \times \left(\frac{7.06 \times 10^{-4}}{2}\right)}{3(20)} = 2.35 \times 10^{-4} < 0.1$$

\Rightarrow lumped assumption is correct

$$\frac{T - T_\infty}{T_i - T_\infty} = e^{-t/\tau}$$

$$\frac{199 - 200}{25 - 200} = e^{-t/1} \Rightarrow t = 5.16 \text{ sec.}$$

