# Torsion of Thin-Walled Tubes

The torque applied to thin-walled tubes is expressed as



where T is the torque in N·mm, A is the area enclosed by the centerline of the tube (as shown in the stripefilled portion) in  $mm^2$ , and q is the shear flow in N/mm.

The average shearing stress across any thickness t is

$$\tau = \frac{q}{t} = \frac{T}{2At}.$$

Thus, torque T ca also be expressed as

 $T = 2At\tau$ .

# Solved Problems in Torsion of Thin-Walled Tubes

#### Problem 337

A torque of 600 N·m is applied to the rectangular section shown in Fig. P-337. Determine the wall thickness t so as not to exceed a shear stress of 80 MPa. What is the shear stress in the short sides? Neglect stress concentration at the corners.

## Solution 337

```
T = 2At\tau
Where: T = 600 N·m = 600 000 N·mm

\land 30(90) 2400 mm<sup>2</sup>

\tau = 80 MPa

600 000 - 2(2400)(t)(80)

t = 1.5625 mm
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At any convenient center *O* within the section, the farthest side is the shortest side, thus, it is induced with the maximum allowable shear stress of **80 MPa**.

# Problem 338

A tube 0.10 in. thick has an elliptical shape shown in Fig. P-338. What torque will cause a shearing stress of 8000 psi?



## Solution 338





# Problem 339

A torque of 450 lb·ft is applied to the square section shown in Fig. P-339. Determine the smallest permissible dimension a if the shearing stress is limited to 6000 psi.



Figure P-339

### Solution 339

$$T = 2At\tau$$
Where: T = 450 lb·ft  
T = 450(12) lb·in  
A = a<sup>2</sup>  
 $\tau$  = 6000 psi  
450(12) = 2a<sup>2</sup>(0.10)(6000)  
a = 2.12 in

# Problem 340

A tube 2 mm thick has the shape shown in Fig. P-340. Find the shearing stress caused by a torque of 600 N·m.

## Solution 340

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T = 2At\tau
Where: A = \pi(10^2) + 80(20) = 1914.16 \text{ mm}^2
t = 2 \text{ mm}
T = 600 \text{ N·m} = 600 000 \text{ N·mm}
600 000 = 2(1914.16)(2)\tau
\tau = 78.36 \text{ MPa}
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## Problem 341

Derive the torsion formula  $\tau = T_p/J$  for a solid circular section by assuming the section is composed of a series of concentric thin circular tubes. Assume that the shearing stress at any point is proportional to its radial distance.

## Solution 341

$$T = 2At\tau$$
Where:  $T = dT$ ;  $A = \pi\rho^2$ ;  $t = d\rho$   
 $\frac{\tau}{\rho} = \frac{\tau_{max}}{r}$ ;  $\tau = \frac{\tau_{max}\rho}{r}$   
 $dT = 2\pi(\rho^2) d\rho \left(\frac{\tau_{max}\rho}{r}\right)$   
 $T = \frac{2\pi\tau_{max}}{r} \int_0^r \rho^3 d\rho$   
 $T = \frac{2\pi\tau_{max}}{r} \left[\frac{\rho^4}{4}\right]_0^r$   
 $T = \frac{2\pi\tau_{max}}{r} \left(\frac{r^4}{4}\right)$   
 $T = \frac{\tau_{max}}{r} \left(\frac{\pi r^4}{2}\right)$   
 $T = \frac{\tau_{max}}{r} J$   
 $\tau_{max} = \frac{Tr}{J}$  and it follows that  $\tau = \frac{T\rho}{J}$ 

# **Helical Springs**

When close-coiled helical spring, composed of a wire of round rod of diameter d wound into a helix of mean radius R with n number of turns, is subjected to an axial load P produces the following stresses and elongation:



The maximum shearing stress is the sum of the direct shearing stress  $\tau_1 = P/A$  and the torsional shearing stress  $\tau_2 = Tr/J$ , with T = PR.

$$\tau = \tau_1 + \tau_2 = \frac{P}{\pi d^2 / 4} + \frac{16(PR)}{\pi d^3}$$
$$\tau = \frac{16PR}{\pi d^3} \left(1 + \frac{d}{4R}\right)$$

This formula neglects the curvature of the spring. This is used for light spring where the ratio d/4R is small.

For heavy springs and considering the curvature of the spring, a more precise formula is given by: (A.M.Wahl Formula)

$$\tau = \frac{16PR}{\pi d^3} \left( \frac{4m-1}{4m-4} + \frac{0.615}{m} \right)$$

where m is called the spring index and (4m - 1) / (4m - 4) is the Wahl Factor.

The elongation of the bar is

$$\delta = \frac{64PR^3n}{Gd^4}$$

Notice that the deformation  $\delta$  is directly proportional to the applied load P. The ratio of P to  $\delta$  is called the spring constant k and is equal to

$$k = \frac{P}{\delta} = \frac{Gd^4}{64R^3n}$$
 in N/mm