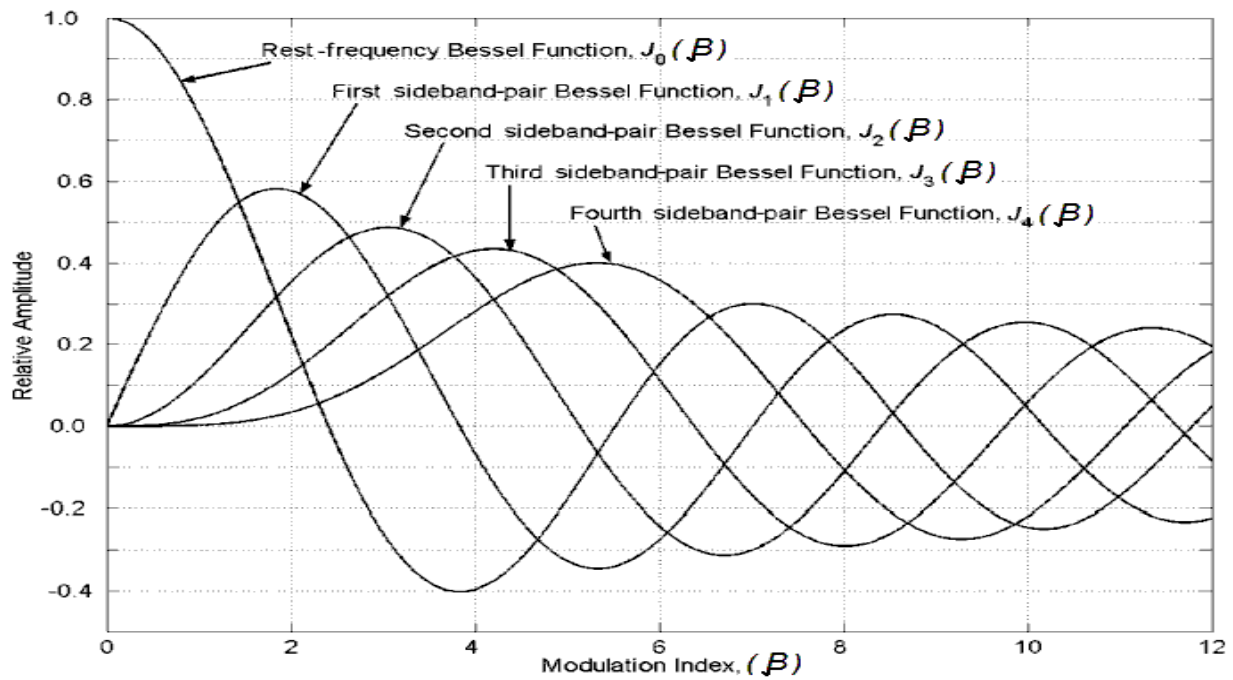


Table of Bessel function

x	Bessel-function order, n																
	J_0	J_1	J_2	J_3	J_4	J_5	J_6	J_7	J_8	J_9	J_{10}	J_{11}	J_{12}	J_{13}	J_{14}	J_{15}	J_{16}
0.00	1.00	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
0.25	0.98	0.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
0.5	0.94	0.24	0.03	—	—	—	—	—	—	—	—	—	—	—	—	—	—
1.0	0.77	0.44	0.11	0.02	—	—	—	—	—	—	—	—	—	—	—	—	—
1.5	0.51	0.56	0.23	0.06	0.01	—	—	—	—	—	—	—	—	—	—	—	—
2.0	0.22	0.58	0.35	0.13	0.03	—	—	—	—	—	—	—	—	—	—	—	—
2.41	0	0.52	0.43	0.20	0.06	0.02	—	—	—	—	—	—	—	—	—	—	—
2.5	-0.05	0.50	0.45	0.22	0.07	0.02	0.01	—	—	—	—	—	—	—	—	—	—
3.0	-0.26	0.34	0.49	0.31	0.13	0.04	0.01	—	—	—	—	—	—	—	—	—	—
4.0	-0.40	-0.07	0.36	0.43	0.28	0.13	0.05	0.02	—	—	—	—	—	—	—	—	—
5.0	-0.18	-0.33	0.05	0.36	0.39	0.26	0.13	0.05	0.02	—	—	—	—	—	—	—	—
5.53	0	-0.34	-0.13	0.25	0.40	0.32	0.19	0.09	0.03	0.01	—	—	—	—	—	—	—
6.0	0.15	-0.28	-0.24	0.11	0.36	0.36	0.25	0.13	0.06	0.02	—	—	—	—	—	—	—
7.0	0.30	0.00	-0.30	-0.17	0.16	0.35	0.34	0.23	0.13	0.06	0.02	—	—	—	—	—	—
8.0	0.17	0.23	-0.11	-0.29	-0.10	0.19	0.34	0.32	0.22	0.13	0.06	0.03	—	—	—	—	—
8.65	0	0.27	0.06	-0.24	-0.23	0.03	0.26	0.34	0.28	0.18	0.10	0.05	0.02	—	—	—	—
9.0	-0.09	0.25	0.14	-0.18	-0.27	-0.06	0.20	0.33	0.31	0.21	0.12	0.06	0.03	0.01	—	—	—
10.0	-0.25	0.04	0.25	0.06	-0.22	-0.23	-0.01	0.22	0.32	0.29	0.21	0.12	0.06	0.03	0.01	—	—
12.0	0.05	-0.22	-0.08	0.20	0.18	-0.07	-0.24	-0.17	0.05	0.23	0.30	0.27	0.20	0.12	0.07	0.03	0.01

Bessel function first kind



Ex. 5-3

A given FM transmitter is modulated with a single sinusoid. The output for no modulation is 100 watt, into a 50Ω resistive load. If the power provided for the first sideband is made zero, find:

- Carrier power.
- All sidebands power.
- Average power in second order sidebands.

Solution:

$$P_1 = 0 \Rightarrow J_1(\beta)^2 = 0 \Rightarrow J_1(\beta) = 0, \therefore \beta \cong 3.8$$

$$a) J_1(\beta) = 0 \text{ at } \beta \cong 3.8$$

$$P_c = \frac{1}{2} A_c^2 J_0^2(\beta) = P_t J_0^2(3.8) = 16 \text{ watt}$$

$$b) P_s = P_t - P_c = 100 - 16 = 84 \text{ watt}$$

$$c) P_2 = 2 \left[\frac{1}{2} A_c^2 J_2^2(\beta) \right] = 2 \times 100 \times J_2^2(3.8) = 34 \text{ watt}$$

H.W

A carrier signal given by $10 \cos 2\pi \times 10^8 t$ volt is FM modulated by single tone message $4 \cos 2\pi \times 10^3 t$ volt if the modulation constant is $1000 \frac{\text{Hz}}{\text{Volt}}$,

- Compute max. frequency deviation and deviation ratio.
- Write the equation of modulated wave.
- Sketch the spectrum.
- Calculate sidebands carrier and total power.

Generation of Wideband FM signals

1- Indirect method (Armstrong Method)

In this method, a NBFM signal is first generated with small β (modulation index) then increased using frequency multiplier (nonlinear device and BPF).

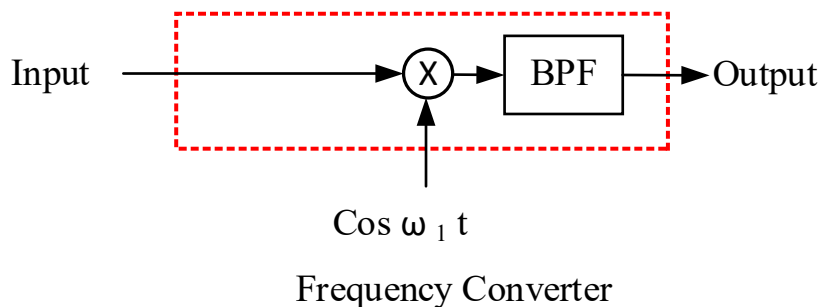
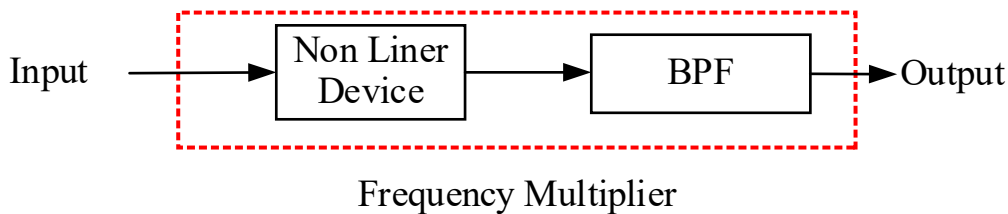
$$\begin{aligned}
 e_i(t) &= A_c \cos(\omega_c t + \beta \sin \omega_m t) \\
 e_o(t) &= a e_i^2(t) \\
 &= a A_c^2 \cos^2(\omega_c t + \beta \sin \omega_m t) \\
 &= \left(\frac{1}{2}\right) a A^2 [1 + \cos(2\omega_c t + 2\beta \sin \omega_m t)], \text{ where } \omega_c \text{ and } \beta \text{ are doubled.}
 \end{aligned}$$

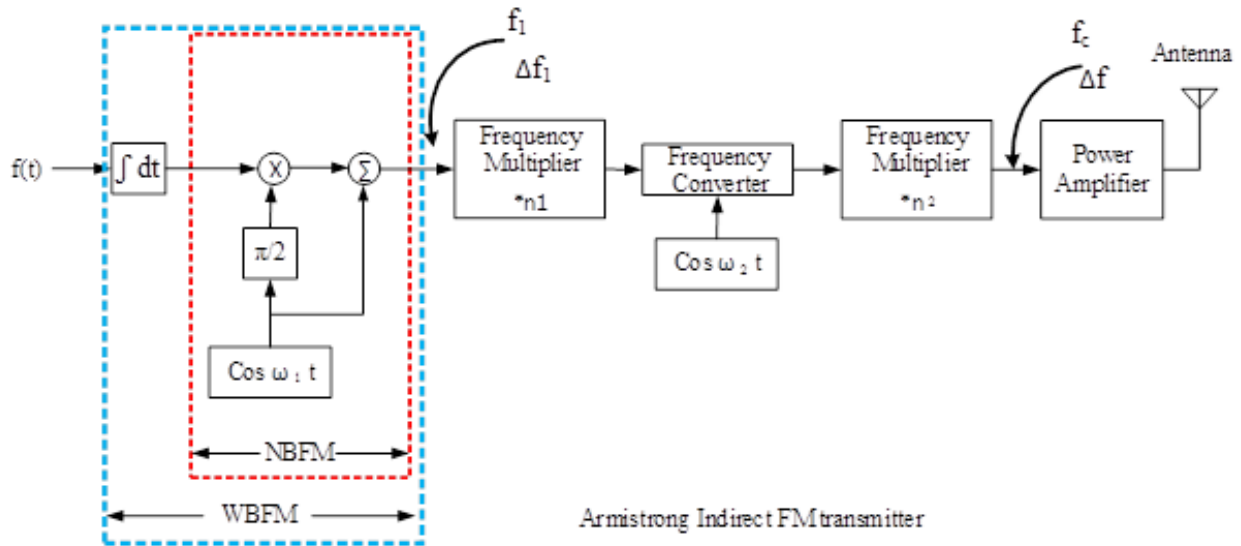
Using a nonlinear device with I/O c/cs:

$$e_o(t) = a_0 + a_1 e_i(t) + a_2 e_i^2(t) + \dots + a_n e_i^n(t)$$

Then we will have $n\beta$, i.e. WBFM,

But we also have $n\omega_c$. Therefore we use frequency convertor to control the value of ω_c .





The frequency deviation is given by: $\Delta f = n_1 n_2 \Delta f_1$... (5-27)

And the carrier frequency is: $f_c = (n_1 f_1 \pm f_2) n_2$... (5-28)

Practically the value of Δf_1 is 25 Hz, in order to maintain $\beta \ll 1$ (as required in NBFM), the balanced spectrum range from 50 Hz to 15 kHz (audio frequencies).

$$\beta = \frac{\Delta f}{f_m}, \text{ at } f_m = 15 \text{ kHz} \Rightarrow \beta = \frac{25}{15k} = 0.00167$$

$$\text{at } f_m = 50 \text{ Hz} \Rightarrow \beta = \frac{25}{50} = 0.5, \text{ Worse possible case}$$

The two values of carrier frequency due to positive and negative signs are compared with the FM band [88 MHz to 108 MHz], so we choose the value which lies in that range.

The values n_1 & n_2 are chosen such that they can be generated using doublers and triplers I cascaded more easier practically

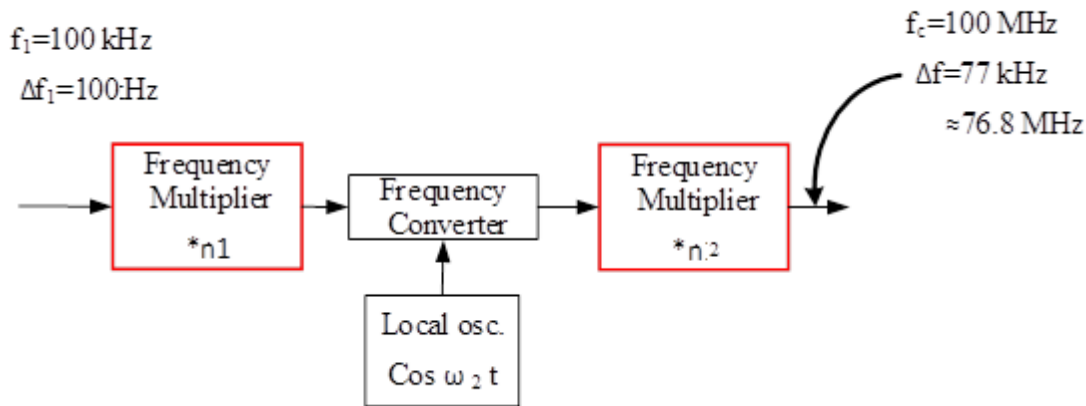
(ex. $64 = 2 \times 2 \times 2 \times 2 \times 2 \times 2$, $48 = 2 \times 2 \times 2 \times 2 \times 3$,)

Ex 5-4

Consider the signal $2 \cos(2\pi \times 10^5 t + 0.1 \sin 2\pi \times 10^3 t)$ is used to generate WBFM with Δf no more than 77 kHz, and f_c of 100 MHz.

- Design a circuit of Armstrong transmitter.
- Determine an estimate of BW of both signals.

Solution



$$\beta = 0.1$$

$$f_m = 10^3 = 1 \text{ kHz}$$

$$\Delta f_1 = \beta f_m = 0.1 \times 10^3 = 100 \text{ Hz}$$

$$n = \frac{77 \text{ kHz}}{100 \text{ Hz}} = 770$$

$$n \cong 2^8 \times 3 = 768$$

Say $n_1 = 2^5 = 32$

$n_2 = 2^3 \times 3 = 24$

$$\Delta f = n_1 n_2 \Delta f_1 = 768 \times 100 \text{ Hz}$$

$$= 76.8 \text{ kHz}$$

2	770
2	385
2	384
2	192
2	96
2	48
2	24
2	12
2	6
3	3
	1

$$f_c = (n_1 f_1 \pm f_2) n_2$$

Since $n_1 n_2 f_1 = 768 * 100 \text{ k} = 76.8 \text{ MHz}$ which is less than f_c (100 MHz).

The sign in above equation is +, i.e:

$$f_c = (n_1 f_1 + f_2) n_2$$

$$100 * 10^6 = (32 * 100 * 10^3 + f_2) * 24$$

$$f_2 = 33.2 \text{ MHz.}$$

$$\text{a) } BW_{\text{NBFM}} = 2f_m = 2 \text{ kHz}$$

$$BW_{\text{WBFM}} = 2\Delta f = 153.6 \text{ kHz}$$

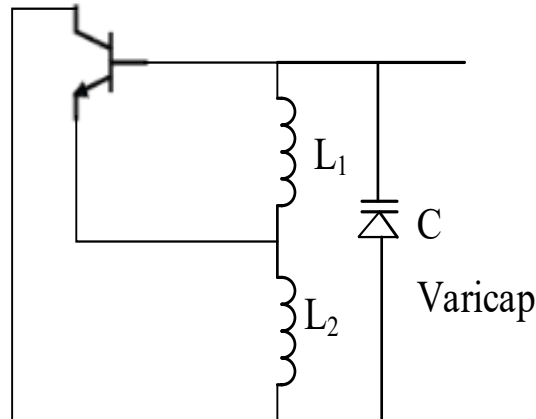
2- Direct Method

Using simple LC oscillator by varying either C or L, depending on the message signal, the frequency generated is ω_c . e.g. Hartly oscillator.

$$\omega_o = \frac{1}{\sqrt{LC}}, \quad L = L_1 + L_2$$

$$c = c_o + kf(t)$$

$$\omega_o = \frac{1}{\sqrt{LC_o \left[1 + \frac{kf(t)}{c_o} \right]}}$$



$$\omega_o = \frac{1}{\sqrt{LC \left[1 + \frac{kf(t)}{c_o} \right]^{1/2}}} \cong \frac{1}{\sqrt{LC_o}} \left[1 + \frac{kf(t)}{2c_o} \right], \quad \text{when } \frac{kf(t)}{c_o} \ll 1$$

Using binomial $(1 + x)^n \cong 1 + nx$ for $x \ll 1$

$$\omega_o = \omega_c \left[1 + \frac{kf(t)}{2c_o} \right] \quad ; \quad \omega_c = \frac{1}{\sqrt{LC_o}}$$

$$\boxed{\omega_o = \omega_c + kf f(t)} \quad \dots (5-29)$$

$$; k_f = \frac{\omega_c k}{2c_o} \dots (5-30)$$

Demodulation of FM Signals

1- Direct method (Discrimination)

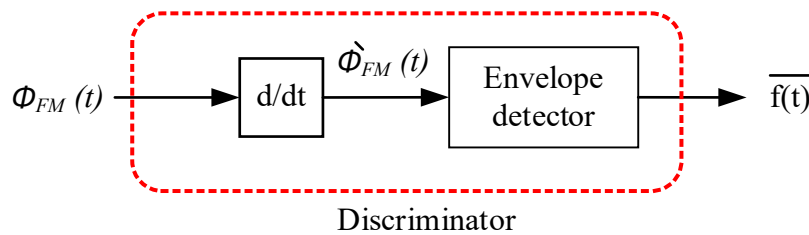
Using differentiator and envelope detector

$$\phi_{FM}(t) = A_c \cos \left[\omega_c t + k_f \int_{-\infty}^t f(\alpha) d\alpha \right]$$

$$\frac{d\phi_{FM}(t)}{dt} = A_c [\omega_c + k_f f(t)] \sin \left[\omega_c t + k_f \int_{-\infty}^t f(\alpha) d\alpha \right] \dots (5-31)$$

\uparrow \uparrow \uparrow
 Const. Const Const

If $k_f f(t) \ll \omega_c$, then envelope of $\phi_{FM}'(t)$ is $A_c [\omega_c + k_f f(t)]$



In fact, the discriminator changes the FM signal into AM with only the slight difference that the new carrier frequency has some frequency variation.

